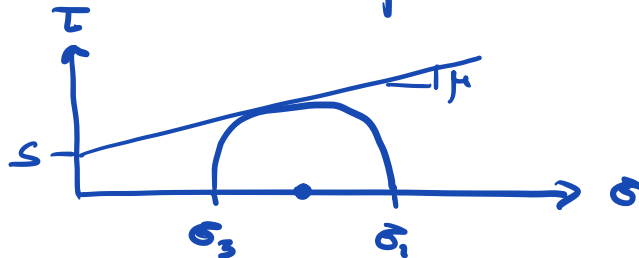


$$(\underline{v} \cdot \nabla) \underline{v} \stackrel{\dot{=}}{=} (\nabla \underline{v}) \underline{v}$$
$$\underline{v} \cdot \nabla \underline{v}$$

Lecture 10: Deformation

- Logistics:
- HW 4 is due Thursday
 - Office hrs tomorrow 3pm

Last time: Mohr circle failure



- Simple states of stress:
hydrostatic, simple & pure shear
plane stress

→ Done with Stress

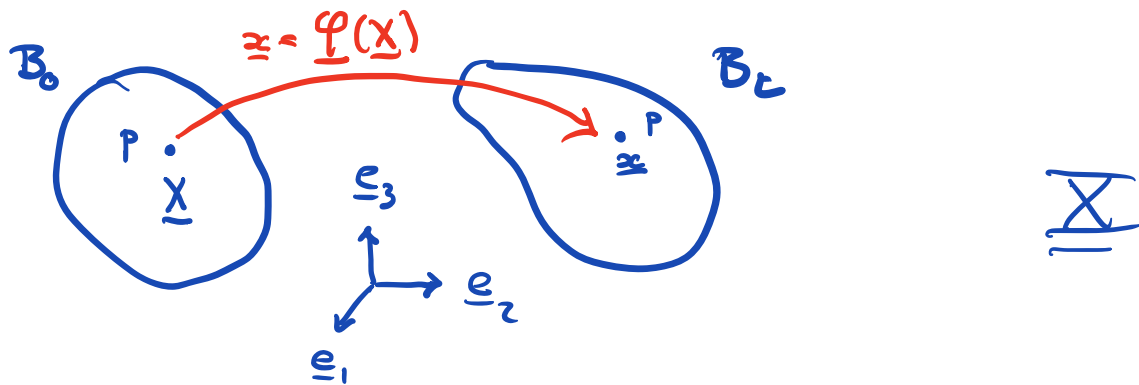
Today: Move to Kinematics

- Deformation mapping
- Measures of Strain
- Deformation gradient

Kinematics

Study of geometry of motion without
~~se~~ considering mass and stress
→ quantify strain and rate of strain

Deformation Mapping



B_0 = body in reference config.

initial, undeformed, material

B_t = body in current, spatial, deformed config

p = material point in body

\underline{X} = location of p in B_0

\underline{x} = location of p in B_t

$\varphi(\underline{X}) =$ deformation mapping

$\{\underline{e}_1, \underline{e}_2, \underline{e}_3\} =$ frame

$\underline{X} = X_I \underline{e}_I$ $X_I =$ components of \underline{X} in $\{\underline{e}_I\}$

$\underline{x} = x_i \underline{e}_i$ $x_i =$ components of \underline{x} in $\{\underline{e}_i\}$

Convention:

Upper case quantities & indices \rightarrow ref. conf B_0

Lower case quantities & " \rightarrow current conf B_t

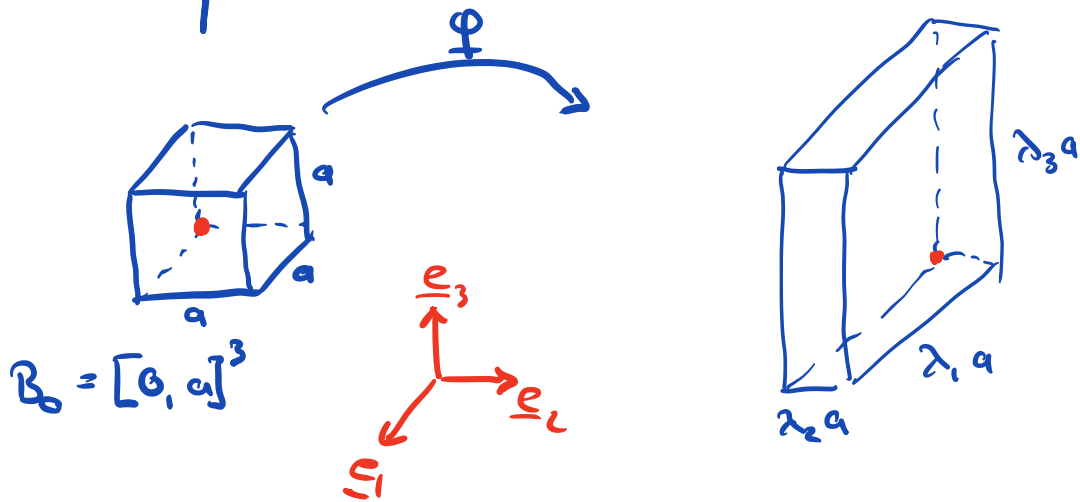
Definition of deformation mapping

$$\underline{x} = \varphi(\underline{X}) = \varphi_i(\underline{X}) \underline{e}_i$$

Displacement of material particle

$$\underline{u}(\underline{X}) = \underline{x} - \underline{X} = \varphi(\underline{X}) - \underline{X}$$

Example: Stretch unit cube



deformation map: $x_1 = \lambda_1 x_1 + v_1$

$$x_2 = \lambda_2 x_2 + v_2$$

$$x_3 = \lambda_3 x_3 + v_3$$

λ : stretch ratios

v_i : translations = 0 $\underline{\underline{\Lambda}} = \begin{bmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \lambda_3 \end{bmatrix}$

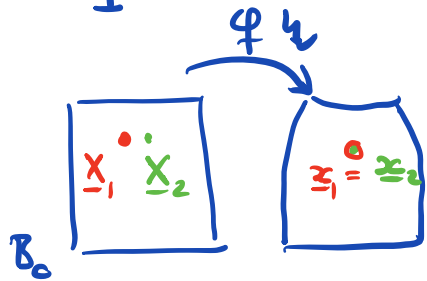
$$\underline{x} = \varphi(\underline{X}) = \lambda_1 X_1 \underline{e}_1 + \lambda_2 X_2 \underline{e}_2 + \lambda_3 X_3 \underline{e}_3$$

$$= \Lambda_{ij} X_j \underline{e}_i = \underline{\underline{\Lambda}} \underline{X}$$

Admissible deformations

For φ to represent a physically feasible deformation it must satisfy two following conditions:

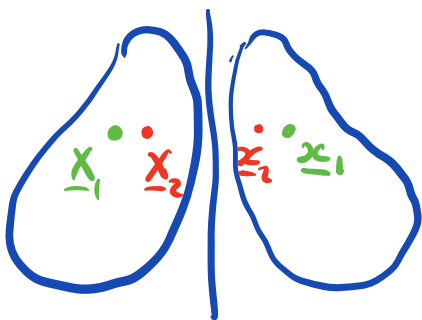
1) $\varphi: B_0 \rightarrow B_t$ has to be "one to one and onto"



Two separate material points in B_0 cannot be mapped to same point in B_t .

2) $\det(\nabla \varphi) > 0 \stackrel{R}{=} \stackrel{U}{-}$

The orientation of a body has to be preserved i.e. no reflections.



$Q =$ is ~~an~~ orthogonal matrix

$$\det(\underline{R} \underline{U}) =$$

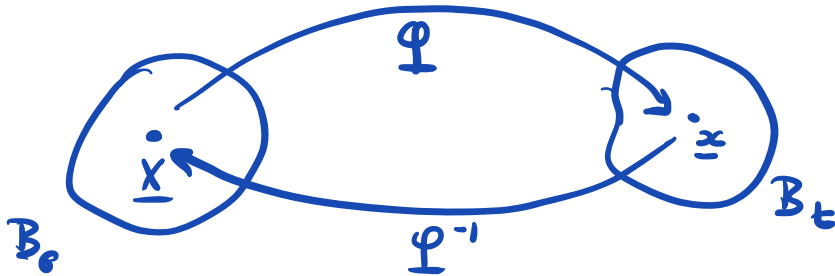
$$\underbrace{\det(\underline{R})}_{\lambda_1 \lambda_2 \lambda_3} \underbrace{\det(\underline{U})}_{> 0}$$

$$\det(Q) > 1 \quad \text{rotation}$$

$$\det(Q) < 1 \quad \text{reflection}$$

Inverse Mapping

If φ is admissible \Rightarrow well defined inverse φ^{-1}



inverse def. map: $\underline{x} = \varphi^{-1}(\underline{x})$

Measures of Strain

In 1D we have simple measures

original: $\overbrace{\hspace{2cm}}^L$ $\Delta L = \ell - L$
deformed: $\overbrace{\hspace{2cm}}^{\ell}$

engineering strain: $e = \frac{\Delta L}{L}$ "relative def."

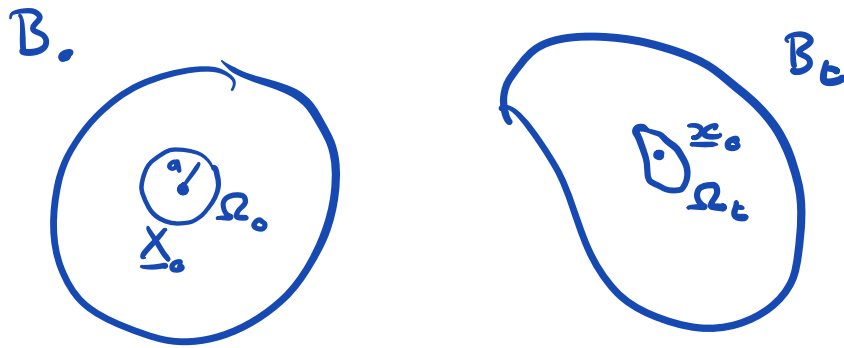
stretch ratio: $\lambda = \frac{\ell}{L}$ $e = \lambda - 1$

Henchy strain: $\varepsilon = \ln(\lambda)$

Green strain: $\varepsilon = \frac{1}{2}(\lambda^2 - 1)$

\Rightarrow Quantification of strain is not unique

We are looking for general 3D approach that is not limited to small deformations.



Sphere of radius a around \underline{x}_0 , is

mapped to $\Omega_t = \varphi(\Omega_0)$

$$\Omega_t = \{ \underline{x} \in B_t \mid \underline{x} = \varphi(\underline{x}), \underline{x}_0 \in \Omega_0 \}$$

Def: The strain at \underline{x}_0 is any relative difference between Ω_0 and Ω_t in limit of $a \rightarrow 0$.

Deformation Gradient

Natural way to quantify strain near \underline{x}_0

$$\underline{\underline{F}}(\underline{x}) = \nabla \varphi(\underline{x})$$

$$F_{i,j} = \frac{\partial \varphi_i}{\partial x_j}$$

Approximate φ using Taylor series around \underline{x}_0

$$\begin{aligned}\varphi(\underline{x}) &= \varphi(\underline{x}_0) + \nabla \varphi(\underline{x}_0) (\underline{x} - \underline{x}_0) + \mathcal{O}(|\underline{x} - \underline{x}_0|^2) \\ &= \underbrace{\varphi(\underline{x}_0) - \nabla \varphi(\underline{x}_0) \underline{x}_0}_c + \nabla \varphi(\underline{x}_0) \underline{x} \\ &= c + \underline{\underline{F}}(\underline{x}_0) \underline{x}\end{aligned}$$

In vicinity of \underline{x} we have lin. approx

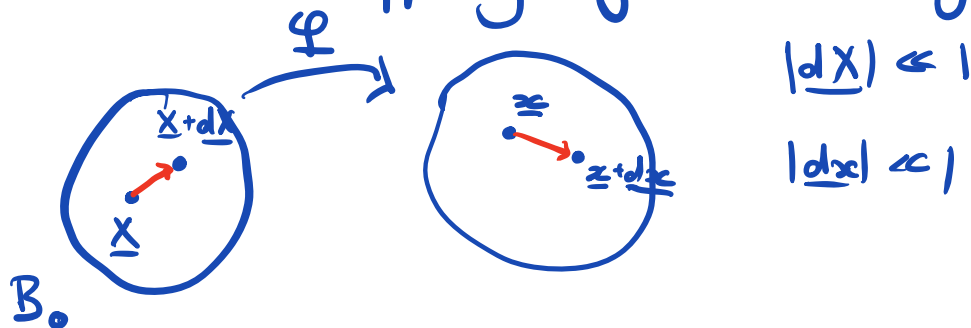
$$\varphi(\underline{x}) = c + \underline{\underline{F}}(\underline{x}) \underline{x}$$

$\Rightarrow \underline{\underline{F}}(\underline{x})$ describes local deformation

Homogeneous def. $\underline{\underline{F}}$ is const.

$$\underline{\underline{x}} = \varphi(\underline{x}) = c + \underline{\underline{F}} \underline{x} \quad \text{affine def.}$$

Consider mapping of a line segment



$$\cancel{x} + \underline{dx} = \varphi(\underline{x} + \underline{dX}) \approx \varphi(\underline{x}) + \underbrace{\nabla \varphi(\underline{x})}_{\underline{F}} \underline{dX}$$

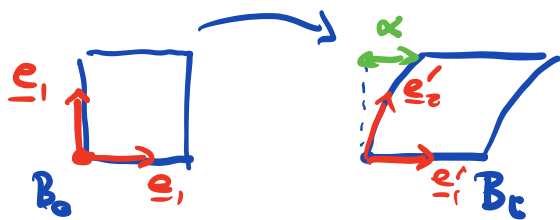
$$\underline{dx} = \underline{F} \underline{dX}$$

$$dx_i = F_{ij} dX_j$$

(conv. def.)

\underline{F} maps material vectors into spatial vectors.

Example: Shear deformation



$$\varphi(\underline{x}) = [x_1 + \alpha x_2^2, x_2]^T$$

$$\frac{\partial \varphi_1}{\partial x_2}$$

$$\nabla \varphi = \begin{bmatrix} 1 & 2\alpha x_2 \\ 0 & 1 \end{bmatrix} = \underline{\underline{F}}(\underline{x})$$

$$\underline{\underline{F}}(\underline{0})\underline{e}_1 = [1, 0]^T \quad \underline{e}_1 \text{ is unchanged}$$

$$\underline{\underline{F}}\underline{e}_2 = [2\alpha x_2, 1]^T$$

In admissible deformation

