

## Lecture 15: Rate of deformation & Reynolds Transport Thm

Logistics: - no HW, my apologies

Last time: - Motions  $\varphi(\underline{x}, t)$  &  $\Psi(\underline{x}, t) = \varphi^{-1}(\underline{x}, t)$

- spatial & material fields  $\Gamma(\underline{x}, t)$   $\Omega(\underline{x}, t)$

spatial and material representations

$$\Gamma_m(\underline{x}, t) = \Gamma(\varphi(\underline{x}, t), t), \Omega_s(\underline{x}, t) = \Omega(\Psi(\underline{x}, t), t)$$

- spatial & material derivatives

$$\dot{\Omega}(\underline{x}, t) = \frac{\partial}{\partial t} \Omega(\underline{x}, t)$$

$$\dot{\Gamma}_s(\underline{x}, t) = \frac{\partial \Gamma}{\partial t} + \underline{v} \cdot \nabla \Gamma$$

spatial representation of material derivative  
of a spatial field!

$\Rightarrow$  independent of  $\varphi$ !

Today: More on rates

- Rate of strain & spin tensors
- Reynolds transport theorem

## Rate of deformation tensors

Velocity gradient takes role of def. gradient

Spatial velocity gradient:

$$\underline{\underline{\ell}} = \nabla_{\underline{x}} \underline{\underline{\omega}}$$

$$\ell_{ij} = \frac{\partial \omega_i}{\partial x_j}$$

Material velocity gradient:

$$\underline{\underline{F}} = \nabla_{\underline{x}} \varphi \quad F_{ij} = \varphi_{i,j}$$

$$\underline{\underline{V}} = \dot{\varphi} \quad v_i = \varphi_{i,t}$$

$$\dot{\underline{\underline{F}}} = \frac{\partial}{\partial t} (\nabla_{\underline{x}} \varphi) = \nabla_{\underline{x}} \left( \frac{\partial \varphi}{\partial t} \right) = \nabla_{\underline{x}} \dot{\underline{\underline{V}}} \quad \dot{F}_{i,j} = v_{i,j}$$

$$\text{Deformation: } \varphi(\underline{x} + \Delta \underline{x}) = \varphi(\underline{x}) + \underline{\underline{F}} \Delta \underline{x}$$

$$\underline{\underline{V}}(\underline{x} + \Delta \underline{x}) = \underline{\underline{V}}(\underline{x}) + \dot{\underline{\underline{F}}} \Delta \underline{x}$$

$$= \underline{\underline{V}}(\underline{x}) + \nabla_{\underline{x}} \underline{\underline{V}} \Delta \underline{x}$$

$$\text{Note: } \underline{\underline{V}}(\underline{x}, t) = \underbrace{\underline{\underline{\omega}}(\varphi(\underline{x}, t), t)}_{\underline{x}}$$

$\underline{\underline{V}}$  and  $\underline{\underline{\omega}}$  are same vector field

just expressed in a different variable

$$\nabla_x \underline{V} \neq \nabla_x \underline{v}|_{x=\varphi(\underline{x}, t)}$$

because gradients are in different directions

$$\dot{\underline{F}}_{ij} = \frac{\partial}{\partial x_j} v_i = \frac{\partial}{\partial x_j} v_i(\varphi(\underline{x}, t), t)$$



where  $\frac{\partial}{\partial x_j} = \frac{\partial}{\partial x_k} \frac{\partial x_k}{\partial x_j} = \frac{\partial}{\partial x_k} \varphi_{k,j} = \frac{\partial}{\partial x_k} F_{kj}$

substitute

$$\dot{\underline{F}}_{ij} = \frac{\partial}{\partial x_k} v_i(x, t) F_{kj} = v_{i,k} F_{kj}$$

$$\dot{\underline{F}} = \nabla_x \underline{V} = \nabla_x \underline{v} \underline{F}$$

$$\Rightarrow \boxed{\dot{\underline{F}} = \nabla_x \underline{v} = \dot{\underline{F}} \underline{F}^{-1}}$$

Need to decompose  $\dot{\underline{F}}$  just like  $\underline{F}$

$$\text{Finite strain } \underline{F} = \underline{B} \underline{U} \quad \nabla \varphi \quad \underline{u} = \varphi - \underline{x}$$

$$\text{infinitesimal strains: } \nabla \underline{u} = \text{sym}(\nabla \underline{u}) + \text{skew}(\nabla \underline{u})$$

## Decomposition of $\underline{\underline{\epsilon}}$

Because we are interested in instantaneous rates of change we can use additive decom.

$$\underline{\underline{\epsilon}}(\underline{x}, t) = \nabla_{\underline{x}} \underline{\underline{\varepsilon}} = \underline{\underline{\dot{\epsilon}}} + \underline{\underline{\omega}}$$

$$\underline{\underline{\dot{\epsilon}}} = \text{sym}(\nabla_{\underline{x}} \underline{\underline{\varepsilon}}) = \frac{1}{2} (\nabla_{\underline{x}} \underline{\underline{\varepsilon}} + \nabla_{\underline{x}} \underline{\underline{\varepsilon}}^T)$$

$$\underline{\underline{\omega}} = \text{skew}(\nabla_{\underline{x}} \underline{\underline{\varepsilon}}) = -\frac{1}{2} (\nabla_{\underline{x}} \underline{\underline{\varepsilon}} - \nabla_{\underline{x}} \underline{\underline{\varepsilon}}^T)$$

rate of strain

spin tensor

Interpretation of  $\underline{\underline{\dot{\epsilon}}}$  and  $\underline{\underline{\omega}}$

$$\underline{\underline{\varepsilon}}(\underline{x} + \underline{\Delta x}) \approx \underline{\underline{\varepsilon}}(\underline{x}) + \nabla_{\underline{x}} \underline{\underline{\varepsilon}} \underline{\Delta x} \quad \nabla \underline{\underline{\varepsilon}} = \underline{\underline{\dot{\epsilon}}} + \underline{\underline{\omega}}$$

$$\approx \underline{\underline{\varepsilon}}(\underline{x}) + \underline{\underline{\dot{\epsilon}}} \underline{\Delta x} + \underline{\underline{\omega}} \underline{\Delta x}$$

$$\underline{\underline{\omega}} = -\underline{\underline{\omega}}^T \rightarrow \text{axial vector} \quad \underline{\underline{\omega}} \underline{\Delta x} = \underline{\omega} \times \underline{\Delta x}$$

$$= \underline{\underline{\varepsilon}}(\underline{x}) + \underline{\underline{\dot{\epsilon}}} \underline{\Delta x} + \underline{\omega} \times \underline{\Delta x}$$

$\underline{\underline{\dot{\epsilon}}}$  is rate of change in shape (strain rate)

$\underline{\underline{\omega}}$  is rate of change in orientation (spin)

$\underline{\omega}$  is angular velocity

verticity:  $\nabla_{\underline{x}} \times \underline{\underline{\varepsilon}} = 2 \underline{\omega}$        $2 \times \text{spin}$

## Relation of $\underline{\underline{\ell}}$ to $\underline{\underline{u}}, \dot{\underline{\underline{u}}}, \underline{\underline{R}}, \dot{\underline{\underline{R}}} (\underline{\underline{F}} = \underline{\underline{R}}\underline{\underline{u}})$

$$\underline{\underline{\ell}} = \underline{\underline{\dot{F}}} \underline{\underline{F}}^{-1}$$

Material derivatives:  $\underline{\underline{F}}^T \quad \underline{\underline{F}}^{-T}$

$$\dot{\underline{\underline{I}}} = \frac{d}{dt}(\underline{\underline{F}}^T \underline{\underline{F}}) = \underline{\underline{\dot{F}}}^T \underline{\underline{F}} + \underline{\underline{F}}^T \underline{\underline{\dot{F}}} = \underline{\underline{0}}$$

$$\dot{\underline{\underline{F}}}^{-1} = \underline{\underline{F}}^T \underline{\underline{\dot{F}}} \underline{\underline{F}}^{-1} = \underline{\underline{F}}^T \underline{\underline{\ell}}$$

$$\dot{\underline{\underline{F}}}^{-T} = (\dot{\underline{\underline{F}}}^{-1})^T = (\underline{\underline{F}}^T \underline{\underline{\ell}})^T = \underline{\underline{\ell}} \underline{\underline{F}}^{-T}$$

$$\boxed{\dot{\underline{\underline{F}}}^{-1} = \underline{\underline{F}}^T \underline{\underline{\ell}}}$$

$$\boxed{\dot{\underline{\underline{F}}}^{-T} = \underline{\underline{\ell}} \underline{\underline{F}}^{-T}}$$

substitute  $\underline{\underline{F}} = \underline{\underline{R}}\underline{\underline{u}}$  into  $\underline{\underline{\ell}} = \dot{\underline{\underline{F}}}^{-1}$

$$\begin{aligned} \underline{\underline{\ell}} &= \frac{d}{dt}(\underline{\underline{R}}\underline{\underline{u}}) \underline{\underline{F}}^{-1} = (\dot{\underline{\underline{R}}}\underline{\underline{u}} + \underline{\underline{R}}\dot{\underline{\underline{u}}})(\underline{\underline{R}}\underline{\underline{u}})^{-1} \\ &= (\quad \text{"} \quad ) \underline{\underline{u}}^T \underline{\underline{R}}^{-T} \\ &= \underbrace{\dot{\underline{\underline{R}}}\underline{\underline{u}} \underline{\underline{u}}^T}_{\underline{\underline{I}}} \underline{\underline{R}}^{-T} + \underline{\underline{R}}\dot{\underline{\underline{u}}} \underline{\underline{u}}^{-1} \underline{\underline{R}}^{-T} \end{aligned}$$

$$\underline{\underline{\ell}} = \dot{\underline{\underline{R}}} \underline{\underline{R}}^{-T} + \underline{\underline{R}} \dot{\underline{\underline{u}}} \underline{\underline{u}}^{-1} \underline{\underline{R}}^{-T}$$

$$\text{show } \dot{\underline{\underline{R}}} \underline{\underline{R}}^{-T} = -(\dot{\underline{\underline{R}}}\underline{\underline{R}})^T \quad \frac{d}{dt}(\underline{\underline{R}}^T \underline{\underline{R}}) = \underline{\underline{0}}$$

second term is in general not symmetric

$$\underline{\underline{\ell}} = \underline{\underline{d}} + \underline{\underline{\omega}}$$

$$\underline{\underline{d}} = \text{sym}(\underline{\underline{R}} \dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1} \underline{\underline{R}}^T) = \underline{\underline{R}} \text{sym}(\dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1}) \underline{\underline{R}}^T$$

$$\underline{\underline{\omega}} = \dot{\underline{\underline{R}}} \underline{\underline{R}}^T + \underline{\underline{R}} \text{skew}(\dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1}) \underline{\underline{R}}^T$$

Shows that  $\underline{\underline{d}}$  is not a pure rate of strain  
and  $\underline{\underline{\omega}}$  is not a pure rate of rotation

It remains to be seen why we can use  
 $\underline{\underline{d}}$  in shear viscosity.

## Reynolds Transport Thm

motion  $\varphi(\underline{x}, t)$  with  $\underline{v}(\underline{x}, t)$  and

$\Omega_t \subset B_t$  with surface  $\partial\Omega_t$  and  
outward unit normal  $\underline{n}$ .

$$\frac{d}{dt} \int_{\Omega_t} \phi(\underline{x}, t) dV_x = \underbrace{\int_{\Omega_t} \frac{\partial \phi}{\partial t} dV_x}_{\text{change in } \Omega} + \underbrace{\oint_{\partial\Omega_t} \phi \underline{v} \cdot \underline{n} dA_x}_{\text{flux across } \partial\Omega_t \text{ due motion of } \Omega.}$$

Key: Although  $\Omega_t = \varphi(\Omega_0, t)$  we can compute derivative without knowledge of  $\varphi$

Have to reference config.

$$\frac{d}{dt} \int_{\Omega_t} \phi(\underline{x}, t) dV_x = \frac{d}{dt} \int_{\Omega_0} \underbrace{\phi(\varphi(\underline{x}, t), t)}_{\phi_m(\underline{x}, t)} J(\underline{x}, t) dV_x$$

$\Omega_0$  is fixed exchange deriv. & integral

$$\int_{\Omega_0} \frac{d}{dt} (\phi_m J) dV_x = \int_{\Omega_0} (\dot{\phi}_m J + \phi_m \dot{J}) dV_x$$

where  $\dot{\mathbf{J}} = \mathbf{J} (\nabla_{\mathbf{x}} \cdot \underline{\underline{\boldsymbol{\sigma}}})_m \rightarrow$  show law

$$= \int_{\Omega_t} \dot{\phi}_m \mathbf{J} + \phi_m \mathbf{J} (\nabla_{\mathbf{x}} \cdot \underline{\underline{\boldsymbol{\sigma}}})_m dV_x$$

$$= \int_{\Omega_t} \dot{\phi}_m + \phi_m (\nabla_{\mathbf{x}} \cdot \underline{\underline{\boldsymbol{\sigma}}})_m \underbrace{\mathbf{J} dV_x}_{dV_x}$$

$$= \int_{\Omega_t} \dot{\phi} + \phi \nabla_{\mathbf{x}} \cdot \underline{\underline{\boldsymbol{\sigma}}} dV_x$$

subst. spatial descrip. of material deriv

$$\dot{\phi} = \frac{\partial \phi}{\partial t} + \underline{\underline{\boldsymbol{\sigma}}} \cdot \nabla_{\mathbf{x}} \phi$$

$$= \int_{\Omega_t} \frac{\partial \phi}{\partial t} + \nabla_{\mathbf{x}} \cdot (\phi \underline{\underline{\boldsymbol{\sigma}}}) dV_x$$

divergence thm

$$= \int_{\Omega_t} \frac{\partial \phi}{\partial t} dV_x + \oint_{\partial \Omega} \phi \underline{\underline{\boldsymbol{\sigma}}} \cdot \underline{\underline{n}} dA_x \checkmark$$

What about  $\dot{\mathbf{J}} = \mathbf{J} (\nabla_{\mathbf{x}} \cdot \underline{\underline{\boldsymbol{\sigma}}})_m ? \quad \mathbf{J} = \det(\underline{\underline{F}})$

From lecture 5:

Deriv. of a scalar valued tensor fun:

$$\dot{\psi}(\underline{\underline{s}}(t)) = D\psi(\underline{\underline{s}}) : \dot{\underline{\underline{s}}}$$

Deriv. of determinant:  $D \det(\underline{S}) = \det(\underline{S}) \underline{S}^T$

From lecture 3:  $\underline{S} : \underline{D} = \text{tr}(\underline{S}^T \underline{D})$

$$\Rightarrow J = \frac{d}{dt} \det(\underline{F}) = \det(\underline{F}) \underline{F}^{-1} : \dot{\underline{F}} = J \text{tr}(\underline{F}^{-1} \dot{\underline{F}})$$
$$= J \text{tr}(\dot{\underline{F}} \underline{F}^{-1})$$

using:  $\nabla_{\underline{x}} \underline{v} = \dot{\underline{F}} \underline{F}^{-1}$

$$J = J \text{tr}(\nabla_{\underline{x}} \underline{v}) = J (\nabla_{\underline{x}} \cdot \underline{v})_m$$