

Lecture 7: Cauchy Stress & Equilibrium

Logistics: - HW 3 is due

- no HW this week

Lost time: - Mass density $\rho(x) = \lim_{\delta \rightarrow 0} \frac{m_{\delta s}}{V_{\delta s}}$

- Centers of volume / mass

- Body forces b $\frac{\text{Force}}{\text{Vol}}$ ρb $\frac{\text{Force}}{\text{mass}}$

- Surface forces (internal & external)

- resultant force & torque (moment)

- traction field t

- Cauchy's postulate $t = t(n(x), x)$

- Action and Reaction $t(-n, x) = -t(n, x)$

- Example: Archimedes principle

Today: - Cauchy's theorem \rightarrow existence of $\underline{\underline{\sigma}}$

- Equilibrium equations

- Stress ellipsoid

Stress tensor

Cauchy's theorem

Let $\underline{\underline{t}}(\underline{n}, \underline{x})$ be a traction field for body B that satisfies Cauchy's postulate. Then $\underline{\underline{t}}$ is linear in \underline{n} , that is, for any $\underline{x} \in B$ there is a sec. ord. tensor field $\underline{\underline{\sigma}}(\underline{x}) \in V^2$ s.t.

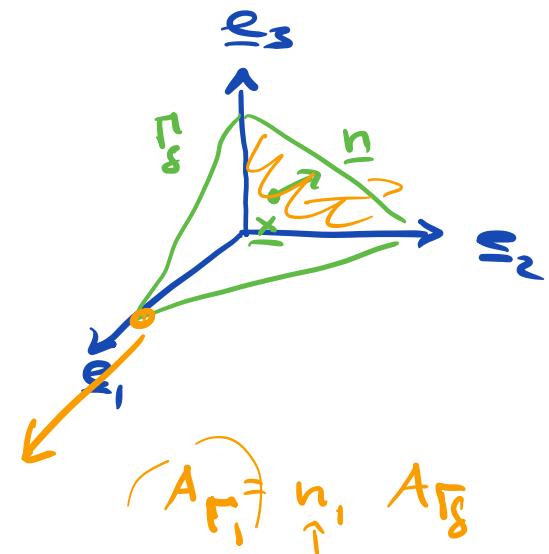
$$\underline{\underline{t}}(\underline{n}, \underline{x}) = \underline{\underline{\sigma}}(\underline{x}) \underline{n}$$

where $\underline{\underline{\sigma}}(\underline{x})$ is the Cauchy stress field.

Frame $\{\underline{e}_i\}$

point \underline{x} with normal \underline{n}
s.t. $\underline{n} \cdot \underline{e}_i \geq 0$

Γ_8 is triangle with
center \underline{x} & normal \underline{n}
max. edge length is s



Ω_δ tetrahedron bounded by Γ_δ

and the coordinate planes Γ_i

with out ward normal $\underline{n}_j = -\underline{e}_j$

$$\partial\Omega_\delta = \Gamma_\delta \cup \Gamma_1 \cup \Gamma_2 \cup \Gamma_3$$

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\partial\Omega_\delta}} \int_{\partial\Omega_\delta} \underline{t}(\underline{n}, \underline{x}) dA = 0 \quad \downarrow$$

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\partial\Omega_\delta}} \left[\int_{\Gamma_\delta} \underline{t}(\underline{n}, \underline{x}) dA + \sum_{j=1}^3 \int_{\Gamma_j} \underline{t}(-\underline{e}_j, \underline{x}) dA \right] = 0$$

Each Γ_j can be linearly mapped into Γ_δ

with const Jacobian.

$$n_j = \underline{n} \cdot \underline{e}_j \geq 0 \Rightarrow A_{\Gamma_j} = n_j A_{\Gamma_\delta}$$

$$\Rightarrow dA_{\Gamma_j} = n_j dA_{\Gamma_\delta}$$

$$A_{\partial\Omega_\delta} = A_{\Gamma_\delta} + \sum_{j=1}^3 A_{\Gamma_j} = \lambda A_{\Gamma_\delta} \quad \lambda = 1 + \sum_{j=1}^3 n_j$$

substitute

$$\lim_{\delta \rightarrow 0} \frac{1}{\lambda A_{\Gamma_\delta}} \int_{\Gamma_\delta} \underline{t}(\underline{n}, \underline{x}) + \sum_{j=1}^3 \underline{t}(-\underline{e}_j, \underline{x}) n_j dA = 0$$

as $\delta \rightarrow 0$ Γ_δ shrinks to x

by mean value theorem for integrals

the limit is given by integrated

$$\underline{t}(u, x) + \sum_{j=1}^3 \underline{t}(-e_j, x) n_j = 0$$

$$\underline{t}(u, x) = - \sum_{j=1}^3 \underline{t}(-e_j, x) u_j$$

$$t(u, x) = \sum_{j=1}^3 \underline{t}(e_j, x) u_j$$

summation convention

$$\underline{t}(u, x) = \underline{t}(e_j, x) u_j$$

$$u_j = u \cdot e_j \quad = (e_j \cdot u) \underline{t}(e_j, x)$$

$$(a \otimes b) \cdot c = (b \cdot c) a \quad = (\underbrace{\underline{t}(e_j, x)}_{\underline{G}(x)} \otimes e_j) u$$

$$\Rightarrow \underline{G} = \underline{t}(e_j, x) \otimes e_j$$

$$\text{write } \underline{t}(e_j, x) = t_i(e_j, x) e_i$$

subst

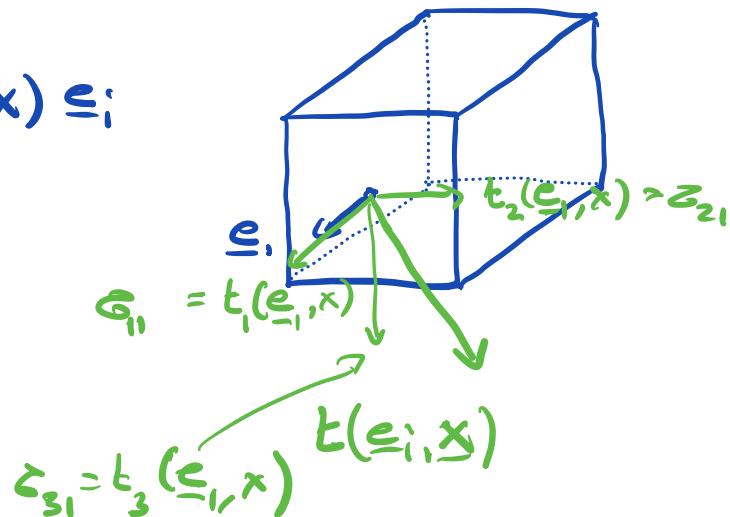
$$\underline{\sigma}(\underline{x}) = \underbrace{t_i(e_j, \underline{x})}_{\sigma_{ij}} e_i \otimes e_j$$

definition of Cauchy stress tensor

$$\underline{\sigma} = \sigma_{ij} e_i \otimes e_j \quad \sigma_{ij} = t_i(e_j, \underline{x})$$

Hence σ_{ij} is the i-th component of the traction on the j-th coordinate plane.

$$\begin{aligned} t_i(e_1, \underline{x}) &= t_i(e_1, \underline{x}) e_i \\ &= \sigma_{i1} e_i \end{aligned}$$



$$\begin{aligned} \underline{t} &= \underline{\sigma} \cdot \underline{n} \\ &= \sigma_{ij} n_j e_i \end{aligned}$$

Mechanical equilibrium

Consider body B under influence of
const body force $\underline{\rho}_b$ and an external
traction \underline{t}

Necessary cond. for eqbm
the resultant force and torque vanish
for any subset $\Omega \subset B$.

$$\underline{\Sigma}[\Omega] = \underline{\Gamma}_b[\Omega] + \underline{\Gamma}_s[\Omega] = \int_{\Omega} \underline{\rho}_b dV + \int_{\partial\Omega} \underline{t} dA = 0$$

$$\underline{\tau}[\Omega] = \underline{\Gamma}_b[\Omega] + \underline{\Gamma}_s[\Omega] = \int_{\Omega} \underline{x} \times \underline{\rho}_b dV + \int_{\partial\Omega} \underline{x} \times \underline{t} dA = 0$$

for any Ω

If $\underline{\Sigma}[\Omega] = 0$ then $\underline{\Sigma}[\Omega]$ is independent
of $\Omega \Rightarrow (\underline{x} - \underline{z}) \times \underline{t} = \underline{x} \times \underline{t}$

Local mech. equilibrium equations

If $\underline{\sigma}(\underline{x})$ is differentiable

b and p are continuous

the eqns imply

$$\left. \begin{aligned} \nabla \cdot \underline{\sigma}(\underline{x}) + p(\underline{x}) b(\underline{x}) &= 0 \\ \underline{\sigma}^T(\underline{x}) &= \underline{\sigma}(\underline{x}) \end{aligned} \right\} \text{for all } \underline{x} \in \Omega$$

in components

$$\begin{aligned} \sigma_{ij,j} + pb_i &= 0 \\ \sigma_{ij} &= \sigma_{ji} \end{aligned}$$

Substitute, $\underline{t} = \underline{\sigma} \underline{n}$ into $r[\Omega]$

$$r[\Omega] = \int_{\partial\Omega} \underline{\sigma} \underline{n} dA + \int_{\Omega} pb \underline{b} dV = 0$$

use Tensor div. thm

$$\int_{\Omega} \nabla \cdot \underline{\sigma} + pb \underline{b} dV = 0$$

by the arbitrary ness of $\Omega \Rightarrow$

$$\Rightarrow \nabla \cdot \underline{\underline{\sigma}} + \rho b = 0$$

To establish symmetry of σ subst. int $\underline{\underline{\sigma}}[\Omega]$

$$\underline{\underline{\sigma}}[\Omega] = \int_{\partial\Omega} \underline{x} \times \underline{t} \, dA + \int_{\Omega} \underline{x} \times \underline{\underline{\sigma}} \underline{b} \, dV$$

$$\int_{\partial\Omega} \underline{x} \times (\underline{\underline{\sigma}} \underline{n}) \, dA - \int_{\Omega} \underline{x} \times \nabla \cdot \underline{\underline{\sigma}} \, dV = 0$$

need to turn l.h.s into \int_{Ω}

$$\text{rewrite } \underline{x} \times (\underline{\underline{\sigma}} \underline{n}) = \underline{\underline{R}} \underline{n}$$

$$\text{where } R_{il} = \epsilon_{ijk} x_j \delta_{kl}$$

$$\int_{\partial\Omega} \underline{\underline{R}} \underline{n} \, dA - \int_{\Omega} \underline{x} \times \nabla \cdot \underline{\underline{\sigma}} \, dV = 0$$

using tensor div. then $\int_{\partial\Omega} \underline{\underline{R}} \underline{n} \, dA = \int_{\Omega} \nabla \cdot \underline{\underline{R}} \, dV$

$$\rightarrow \int_{\Omega} \nabla \cdot \underline{\underline{R}} - \underline{x} \times \nabla \cdot \underline{\underline{\sigma}} \, dV = 0$$

in components

$$\underbrace{(\epsilon_{ijk} \times_j \sigma_{kl})}_{R_{il,L}} - \epsilon_{ijk} \times_j \sigma_{kl,L}$$

chain rule

$$\epsilon_{ijk} \times_{j,L} \sigma_{kl} + \epsilon_{ijk} \times_j \sigma_{kl,L} - \epsilon_{ijk} \times_j \overset{\circ}{\sigma}_{kl,L} = 0$$

$$\epsilon_{ijk} \times_{j,L} \sigma_{kl} = \epsilon_{ijk} \delta_{jl} \sigma_{kl} = \epsilon_{ijk} \sigma_{kj} = 0$$

If $\epsilon_{ijk} \sigma_{kj} = 0$ then $\epsilon_{ihj} \sigma_{jk} = 0$

because j & h are dummy's.

$$\epsilon_{ijk} \sigma_{kj} + \epsilon_{ikj} \sigma_{jk} = 0$$

$$\epsilon_{ijk} (\sigma_{kj} - \sigma_{jk}) = 0$$

we can i separate from j & k

$$\sigma_{kj} - \sigma_{jk} = 0$$

$$\Rightarrow \sigma_{kj} = \sigma_{jk} \quad \sigma^T = \sigma$$

local Eqs

$$\nabla \cdot \underline{\sigma} + P \underline{b} = 0 \quad \left. \begin{array}{l} 3 \text{ equ} \\ 3 \text{ equ} \end{array} \right\} 6 \text{ eqns}$$
$$\underline{\sigma}^T = \underline{\phi}$$

$$\sigma_{12} = \sigma_{21}, \quad \sigma_{13} = \sigma_{31}, \quad \sigma_{23} = \sigma_{32}$$

but $\underline{\sigma}$ has 9 unknown components

\Rightarrow need a constitutive law

$\underline{\sigma} \rightarrow$ \underline{u} displacement
 \underline{v} velocity