

Isothermal Fluid Mechanics

→ application of Eulerian balance laws

→ neglect thermal effects.

10 equations:

$$\dot{\underline{v}}_m = \dot{\underline{\varphi}} \quad 3 \text{ kinematic}$$

$$\frac{\partial \rho}{\partial t} + \nabla_{\underline{x}} \cdot (\rho \underline{v}) = 0 \quad 1 \text{ mass balance}$$

$$\rho \dot{\underline{v}} - \nabla_{\underline{x}} \cdot \underline{\underline{\sigma}} = \rho \underline{b} \quad 3 \text{ linear mom.}$$

$$\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T \quad 3 \text{ angular mom.}$$

16 unknown quantities

$$\varphi \quad \underline{v} \quad \rho \quad \underline{\underline{\sigma}} \quad 3 + 3 + 1 + 9 = 16$$

Constitutive eqn that relate 6 independent components of $\underline{\underline{\sigma}}$ to $\varphi, \underline{v}, \rho$.

If there is a material constraint this adds both an equation $\gamma = 0$ and an unknown q .

Ideal Fluids

A fluid is ideal if

1) Uniform reference mass density: $\rho_0(\underline{x}) = \rho_0 > 0$

2) Fluid is incompressible: $\nabla_{\underline{x}} \cdot \underline{v} = 0$

3) Cauchy stress is spherical: $\underline{\underline{\sigma}} = -p \underline{\underline{I}}$

\Rightarrow no shear stresses $\underline{t} = \underline{\underline{\sigma}} \underline{n} = -p \underline{n}$

1 + 2 $\Rightarrow \rho(\underline{x}, t) = \rho_0$

substituting into mass balance

$$\cancel{\frac{\partial \rho_0}{\partial t}} + \nabla_{\underline{x}} \cdot (\rho_0 \underline{v}) = 0 \Rightarrow \nabla_{\underline{x}} \cdot \underline{v} = 0$$

substituting into mom. balance

$$\rho_0 \dot{\underline{v}} = \nabla_{\underline{x}} \cdot (-p \underline{\underline{I}}) + \rho_0 \underline{b}$$

where $\dot{\underline{v}} = \frac{\partial \underline{v}}{\partial t} + (\nabla_{\underline{x}} \underline{v}) \underline{v}$ and $\nabla_{\underline{x}} \cdot (-p \underline{\underline{I}}) = -\nabla_{\underline{x}} p$

we obtain closed system for \underline{v} and p

$$\rho_0 \left(\frac{\partial \underline{v}}{\partial t} + (\nabla_{\underline{x}} \underline{v}) \underline{v} \right) = -\nabla_{\underline{x}} p + \rho_0 \underline{b}$$

$$\nabla_{\underline{x}} \cdot \underline{v} = 0$$

Euler
Equations

Note: p has undetermined constant.

Frame Indifference of Euler Equations

The stress field of an ideal fluid is entirely reactive

$$\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^r + \underline{\underline{\sigma}}^a = -p \underline{\underline{I}}$$

$$\Rightarrow \underline{\underline{\sigma}}^r = -p \underline{\underline{I}} \quad \underline{\underline{\sigma}}^a = \underline{\underline{0}}$$

where p is the multiplier associated with the incompressibility constraint. $\nabla_x \cdot \underline{\underline{v}} = 0$

For a constrained model to be frame indifferent both the constraint $\gamma(\underline{\underline{F}}(x,t)) = 0$ and the active stress $\underline{\underline{\sigma}}^a$ must be frame indifferent.

Assuming a superposed rigid motion $\underline{\underline{x}}^* = \underline{\underline{Q}} \underline{\underline{x}} + \underline{\underline{c}}$

$$\bullet \gamma(\underline{\underline{F}}^*) = \det(\underline{\underline{F}}^*) - 1 = \det(\underline{\underline{Q}}) \det(\underline{\underline{F}}) - 1 = \gamma(\underline{\underline{F}})$$

\Rightarrow constraint field is indifferent

$$\bullet \underline{\underline{\sigma}}^a = \underline{\underline{0}} \quad \text{trivially indifferent}$$

\Rightarrow material model for an ideal fluid is frame-indif.

$$\frac{\partial \underline{v}}{\partial t} + (\nabla_{\underline{x}} \times \underline{v}) \times \underline{v} = -\nabla_{\underline{x}} \left(\frac{1}{2} |\underline{v}|^2 + \frac{P}{\rho_0} + \psi \right) = -\nabla_{\underline{x}} H$$

$$H = \frac{1}{2} |\underline{v}|^2 + \frac{P}{\rho_0} + \psi \quad \text{where } \psi = gz \text{ for gravity}$$

H has units of energy/mass

$$E_k = \frac{1}{2} m |\underline{v}|^2 \quad E_g = mgz \quad E_P = m \int_{P_0}^P \frac{dP}{\rho} = m \frac{P - P_0}{\rho_0}$$

$$H = \frac{E}{m} = \frac{E_k}{m} + \frac{E_P}{m} + \frac{E_g}{m} = \frac{1}{2} |\underline{v}|^2 + \frac{P}{\rho_0} + gz$$

Steady flow

$$(\nabla_{\underline{x}} \times \underline{v}) \times \underline{v} = -\nabla_{\underline{x}} H$$

take dot product from left

$$\underline{v} \cdot (\nabla_{\underline{x}} \times \underline{v}) \times \underline{v} = -\underline{v} \cdot \nabla_{\underline{x}} H$$

\uparrow
 pop. to \underline{v}

$$\Rightarrow \underline{v} \cdot \nabla_{\underline{x}} H = 0 \quad \text{Bernoulli's Thm for steady flow}$$

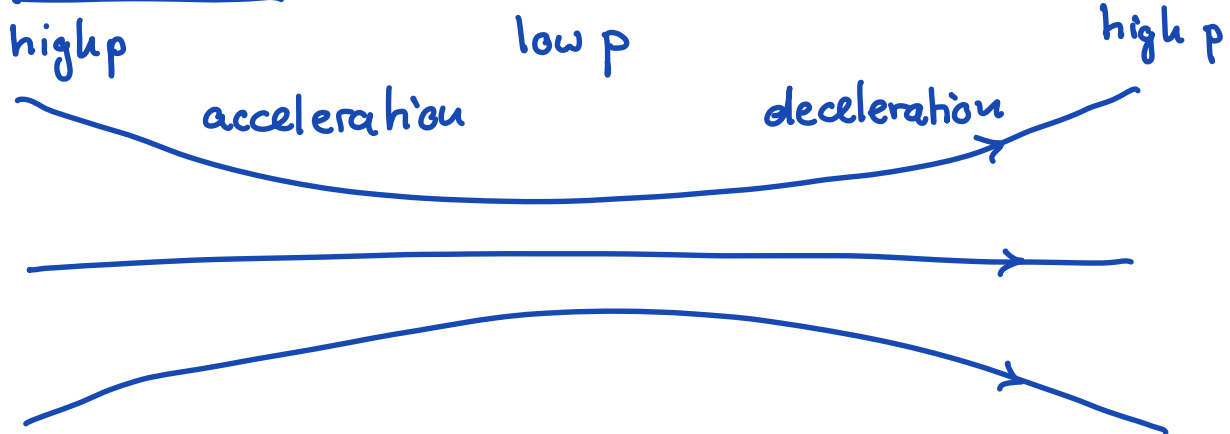
implies that H is constant along a streamline

Stream line is integral curve of \underline{v} .

\Rightarrow Energy is conserved in ideal flow

$$\text{because } \rho \dot{\psi} = \underline{\underline{0}} : \underline{\underline{d}} = 0.$$

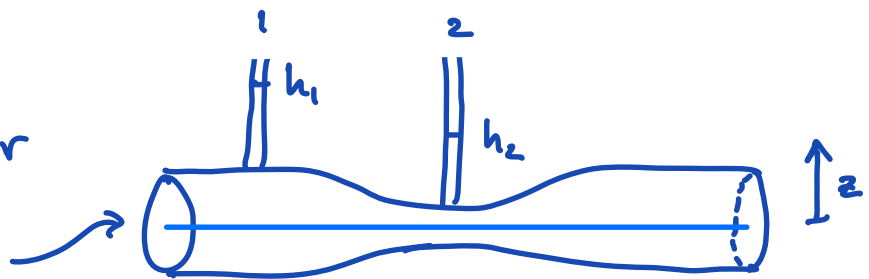
Intuition



Examples:

1) Venturi meter

H is const along



$$H = \frac{p_1}{\rho} + \frac{1}{2} v_1^2 = \frac{p_2}{\rho} + \frac{1}{2} v_2^2 \quad (z=0)$$

$$A_1 v_1 = A_2 v_2 \quad (\text{mass cons.}) \quad v_2 = \frac{A_1}{A_2} v_1$$

$$p_1 - p_2 = \frac{\rho}{2} (v_2^2 - v_1^2) = \frac{\rho}{2} \left(\left(\frac{A_1}{A_2} \right)^2 - 1 \right) v_1^2$$

hydrostatics: $p_1 - p_0 = \rho g h_1$ $p_2 - p_0 = \rho g h_2$

$$\rho g (h_1 - h_2) = \frac{\rho}{2} \left(\frac{A_1^2}{A_2^2} - 1 \right) v_1^2$$

Measure v_1 as:

$$v_1^2 = \frac{2g(h_1 - h_2)}{\left(\frac{A_1^2}{A_2^2} - 1 \right)}$$

Irrotational Motion

A velocity field \underline{v} with spin field $\underline{\underline{W}} = \text{skew}(\nabla_x \underline{v})$ is irrotational if

$$\underline{\underline{W}}(\underline{x}, t) = \underline{\underline{0}} \quad \text{or} \quad \nabla_x \times \underline{v} = \underline{\underline{\omega}} = 0$$

During an irrotational motion material particles experience no net rotation.

Velocity potential

Helmholtz decomposition of velocity

$$\underline{v} = -\nabla_x \phi + \nabla_x \times \underline{\psi}$$

for irrotational flow

$$\nabla_x \times \underline{v} = -\cancel{\nabla_x \times \nabla_x \phi} + \nabla_x \times \nabla_x \times \underline{\psi} = 0$$

$$\Rightarrow \underline{\psi} = \underline{0}$$

ϕ is velocity potential for irrotational flow

$$\underline{v} = -\nabla_x \phi$$

in this case $\nabla_x \cdot \underline{v} = 0 \rightarrow -\nabla_x^2 \phi = 0$ Laplace Eqn.

If the flow is irrotational and steady

$$(\nabla_x \times \underline{v}) \times \underline{v} = -\nabla_x H$$

$$\Rightarrow \boxed{\nabla H = 0}$$

H is constant throughout fluid.

Time dependent irrotational flows

Starting from Euler equation

$$\frac{\partial \underline{v}}{\partial t} + (\nabla_x \times \underline{v}) \times \underline{v} = -\frac{1}{2} \nabla_x |\underline{v}|^2 - \frac{1}{\rho_0} \nabla_x p + \underline{b}$$

substituting $\underline{v} = -\nabla_x \phi$

$$\nabla_x \left(\frac{\partial \phi}{\partial t} + \frac{1}{2} |\underline{v}|^2 + \frac{1}{\rho_0} p - gz \right) = 0$$

which implied that

$$\boxed{\begin{aligned} \frac{\partial \phi}{\partial t} + \frac{1}{2} |\underline{v}|^2 + \frac{p}{\rho_0} - gz &= f(t) \\ -\nabla_x^2 \phi &= 0 \end{aligned}}$$

Bernoulli's Theorem

for irrotational flow

Usefulness hinges on whether irrotational flows are of any real interest.

\Rightarrow understand evolution of vorticity

Vorticity equation

Define vorticity: $\underline{\omega} = \nabla_x \times \underline{v}$

substitute into Euler eqn.

$$\frac{\partial}{\partial t} \underline{v} + \underline{\omega} \times \underline{v} = -\nabla_x H$$

take the curl

$$\frac{\partial}{\partial t} \underline{\omega} + \nabla_x \times (\underline{\omega} \times \underline{v}) = -\cancel{\nabla_x \times} \nabla H = 0$$

expand 2nd term $\underline{\omega} = \omega_i \underline{e}_i$ $\underline{v} = v_j \underline{e}_j$

$$\underline{\omega} \times \underline{v} = \omega_i v_j \underline{e}_i \times \underline{e}_k = \underbrace{\omega_i v_j \epsilon_{ijk}}_{a_k} \underline{e}_k = a_k \underline{e}_k$$

$$\nabla \times \underline{a} = \epsilon_{kmn} a_{k,n} \underline{e}_m$$

$$= \epsilon_{kmn} \epsilon_{ijk} (\omega_i v_j)_{,n} \underline{e}_m$$

$$= \epsilon_{kmn} \epsilon_{kij} (\omega_i v_j)_{,n} \underline{e}_m$$

$$= (\delta_{mi} \delta_{nj} - \delta_{mj} \delta_{ni}) (\omega_i v_j)_{,n} \underline{e}_m$$

$$= \delta_{mi} \delta_{nj} (\omega_i v_j)_{,n} \underline{e}_m - \delta_{mj} \delta_{ni} (\omega_i v_j)_{,n} \underline{e}_m$$

$$= (\omega_i v_j)_{,j} \underline{e}_i - (\omega_i v_j)_{,i} \underline{e}_j$$

$$= \omega_{i,j} v_j \underline{e}_i + \omega_i v_{j,j} \underline{e}_i - \omega_{i,i} v_j \underline{e}_j - v_{j,i} \omega_i \underline{e}_j$$

$$= (\nabla_x \underline{\omega}) \underline{v} + (\cancel{\nabla_x \cdot} \underline{v}) \underline{\omega} - (\cancel{\nabla_x \cdot} \underline{\omega}) \underline{v} - (\nabla_x \underline{v}) \underline{\omega}$$

So that

$$\frac{D}{Dt} \underline{\omega} + (\nabla_x \underline{\omega}) \underline{v} - (\nabla_x \underline{v}) \underline{\omega} = 0$$

identifying material derivative

$$\boxed{\dot{\underline{\omega}} - (\nabla_x \underline{v}) \underline{\omega} = 0} \quad \text{Vorticity equation}$$

Show that an initially irrotational fluid remains irrotational!

Simple 2D proof:

$$\underline{v} = \begin{pmatrix} v_x \\ v_y \\ 0 \end{pmatrix} \quad \nabla_x \underline{v} = \begin{pmatrix} v_{x,x} & v_{x,y} & 0 \\ v_{y,x} & v_{y,y} & 0 \\ 0 & 0 & 0 \end{pmatrix} \quad \underline{\omega} = \nabla_x \times \underline{v} = \begin{pmatrix} 0 \\ 0 \\ \omega \end{pmatrix}$$

$$\boxed{(\nabla_x \underline{v}) \underline{\omega} = 0 \Rightarrow \dot{\underline{\omega}} = 0}$$

The vorticity of a fluid element in an ideal fluid is conserved. Vorticity is conserved along streamlines.

In particular, an ideal fluid initially at rest remains irrotational!

Proof in 3D:

Work in material coords.: $\underline{\omega}_m = \underline{\omega}(\underline{x}, t), t$

Introduce change in variables: $\underline{\omega}_m = \underline{F} \underline{\xi}$ $\underline{\xi} = \underline{F}^{-1} \underline{\omega}_m$

$$\dot{\underline{\omega}} = \frac{\partial}{\partial t} \underline{\omega}_m = \frac{\partial}{\partial t} (\underline{\xi} \underline{F}) = \dot{\underline{F}} \underline{\xi} + \underline{F} \dot{\underline{\xi}}$$

solving for $\dot{\underline{\xi}}$

$$\dot{\underline{\xi}} = \underline{F}^{-1} [\dot{\underline{\omega}}_m - \dot{\underline{F}} \underline{F}^{-1} \underline{\omega}_m]$$

where $\dot{\underline{F}} \underline{F}^{-1} = (\nabla_{\underline{x}} \underline{v})_m$ so that

$$\dot{\underline{\xi}} = \underline{F}^{-1} \underbrace{[\dot{\underline{\omega}}_m - (\nabla_{\underline{x}} \underline{v})_m \underline{\omega}_m]} = 0$$

o vorticity eqn

$$\Rightarrow \dot{\underline{\xi}} = 0 \quad \Rightarrow \underline{\xi}(\underline{x}, t) = \underline{\xi}(\underline{x}, 0)$$

$$\text{since } \underline{F}(\underline{x}, 0) = \underline{I} \Rightarrow \underline{\omega}_m(\underline{x}, 0) = \underline{\xi}(\underline{x}, 0)$$

$$\omega_m(\underline{x}, t) = \underline{F}(\underline{x}, t) \underline{\xi}(\underline{x}, t)$$

$$= \underline{F}(\underline{x}, t) \underline{\xi}(\underline{x}, 0)$$

$$= \underline{F}(\underline{x}, t) \underline{\omega}_m(\underline{x}, 0)$$

$$\text{if } \underline{\omega}_m(\underline{x}, 0) = 0 \Rightarrow \underline{\omega}_m(\underline{x}, t) = 0 \quad \text{!}$$