

# Linear Elasticity

Initial boundary value problem

$$\text{PDE: } \rho_0 \ddot{\varphi} = \nabla_{\underline{x}} \cdot \hat{\underline{P}}(\underline{F}) + \rho_0 \underline{b}_m \quad \underline{x} \in \Omega \times [0, T]$$

$$\text{BC: } \varphi = \underline{g} \quad \partial\Omega_d$$

$$\hat{\underline{P}}(\underline{F}) \underline{N} = \underline{h} \quad \partial\Omega_s$$

$$\text{IC: } \varphi(\underline{x}, 0) = \underline{x} \quad \Omega$$

$$\dot{\varphi}(\underline{x}, 0) = \underline{v}_0 \quad \Omega$$

Consider a stress-free initial condition

$$\text{at } t=0 \quad \underline{F} = \underline{I} \quad \text{so that } \hat{\underline{P}}(\underline{I}) = \hat{\underline{\Sigma}}(\underline{I}) = \hat{\underline{\Sigma}}_m(\underline{I}) = \underline{0}$$

If all the forcings are small

$$|\underline{b}_m| = \mathcal{O}(\varepsilon) \quad |g - x|_{\partial\Omega_d} = \mathcal{O}(\varepsilon) \quad |h| = \mathcal{O}(\varepsilon) \quad |v_0| = \mathcal{O}(\varepsilon)$$

where  $0 < \varepsilon \ll 1$

In this case, we expect displacements to be small

$$|\underline{u}(\underline{x}, t)| = |\varphi(\underline{x}, t) - \underline{x}| = \mathcal{O}(\varepsilon)$$

## Linearized equations

Express forcings as

$$\underline{b}_m^\epsilon = \epsilon \underline{b}_m \quad \underline{g}^\epsilon = \underline{\chi} - \epsilon \underline{g} \quad \underline{h}^\epsilon = \epsilon \underline{h} \quad \underline{v}_0^\epsilon = \epsilon \underline{v}_0$$

then  $\varphi^\epsilon = \underline{\chi} + \epsilon \underline{u} + \mathcal{O}(\epsilon^2)$  where  $\underline{u}^\epsilon = \epsilon \underline{u} = \varphi^\epsilon - \underline{\chi}$

and associated  $\underline{F}^\epsilon = \nabla_{\underline{x}} \varphi^\epsilon = \underline{I} + \epsilon \nabla_{\underline{x}} \underline{u}$

substitute into PDE

$$\rho_0 \frac{\partial^2}{\partial t^2} (\underline{\chi} + \underline{u}^\epsilon) = \nabla_{\underline{x}} \cdot [\hat{\underline{P}}(\underline{F}^\epsilon)] + \rho_0 \underline{b}_m^\epsilon$$

$$\rho_0 \underline{\ddot{u}}^\epsilon = \nabla_{\underline{x}} \cdot [\hat{\underline{P}}(\underline{F}^\epsilon)] + \rho_0 \underline{b}_m^\epsilon$$

Need to deal with  $\nabla_{\underline{x}} \cdot \hat{\underline{P}}(\underline{F})$

Introduce the 4<sup>th</sup>-order tensors

$$A_{ijkl} = \frac{\partial \hat{P}_{ij}}{\partial F_{kl}}(\underline{I}) \quad B_{ijkl} = \frac{\partial \hat{\Sigma}_{ij}}{\partial F_{kl}}(\underline{I}) \quad C_{ijkl} = \frac{\partial \hat{\delta}_{ij}}{\partial F_{kl}}(\underline{I})$$

or in tensor notation the derivatives

$$\mathcal{A}(\underline{H}) = \frac{d}{d\alpha} \hat{\underline{P}}(\underline{I} + \alpha \underline{H}) \Big|_{\alpha=0} = \mathcal{D} \hat{\underline{P}}(\underline{I}) \underline{H}$$

$$\mathcal{B}(\underline{H}) = \frac{d}{d\alpha} \hat{\underline{\Sigma}}(\underline{I} + \alpha \underline{H}) \Big|_{\alpha=0} = \mathcal{D} \hat{\underline{\Sigma}}(\underline{I}) \underline{H}$$

$$\mathcal{C}(\underline{H}) = \frac{d}{d\alpha} \hat{\underline{\delta}}(\underline{I} + \alpha \underline{H}) \Big|_{\alpha=0} = \mathcal{D} \hat{\underline{\delta}}(\underline{I}) \underline{H}$$

Use this to expand stress response

$$\begin{aligned}\hat{\underline{\underline{P}}}(\underline{\underline{F}}^\epsilon) &= \hat{\underline{\underline{P}}}(\underline{\underline{F}}^\epsilon)|_{\epsilon=0} + \epsilon \underline{\underline{A}}(\nabla_x \underline{\underline{u}}) + \mathcal{O}(\epsilon^2) \\ &= \hat{\underline{\underline{P}}}(\underline{\underline{I}}) + \epsilon \underline{\underline{A}}(\nabla_x \underline{\underline{u}}) + \mathcal{O}(\epsilon^2) \\ &= \epsilon \underline{\underline{A}}(\nabla_x \underline{\underline{u}}) + \mathcal{O}(\epsilon^2)\end{aligned}$$

substitute into mom. balance with  $\underline{\underline{u}}^\epsilon = \epsilon \underline{\underline{u}}$  &  $\underline{\underline{b}}_m^\epsilon = \epsilon \underline{\underline{b}}_m$

$$\rho_0 \ddot{\underline{\underline{u}}} = \nabla_x \cdot [\underline{\underline{A}}(\nabla_x \underline{\underline{u}})] + \rho_0 \underline{\underline{b}}_m$$

linearized balance of momentum

$$\boxed{\rho_0 \ddot{\underline{\underline{u}}} = \nabla \cdot [\underline{\underline{A}} \nabla \underline{\underline{u}}] + \rho_0 \underline{\underline{b}}} \quad \text{lin. elasto dynamic eqn.}$$

In linearized case,  $|\varphi - \underline{\underline{x}}| = \mathcal{O}(\epsilon)$  and difference between the current and the reference configuration can be neglected.

If accelerations are zero

$$\boxed{\nabla \cdot [\underline{\underline{A}} \nabla \underline{\underline{u}}] + \rho_0 \underline{\underline{b}} = \underline{\underline{0}}} \quad \text{Elasto static eqn.}$$

(Navier-Cauchy eqbm eqn.)

# Elasticity Tensor

Introduced three 4-th order tensors:

$$\underline{\underline{A}} = D\hat{\underline{\underline{P}}}(\underline{\underline{I}}), \quad \underline{\underline{B}} = D\hat{\underline{\underline{\Sigma}}}(\underline{\underline{I}}) \quad \text{and} \quad \underline{\underline{C}} = D\hat{\underline{\underline{\delta}}}(\underline{\underline{I}})$$

If the reference configuration is stress free

$$\Rightarrow \underline{\underline{A}} = \underline{\underline{B}} = \underline{\underline{C}}$$

Example: Show  $\underline{\underline{A}} = \underline{\underline{C}}$

$$\hat{\underline{\underline{P}}}(\underline{\underline{F}}) = \det(\underline{\underline{F}}) \hat{\underline{\underline{\delta}}}(\underline{\underline{F}}) \underline{\underline{F}}^{-T}$$

differentiating both sides at  $\underline{\underline{F}} = \underline{\underline{I}}$

$$\begin{aligned} \underline{\underline{A}} \underline{\underline{H}} &= \frac{d}{d\epsilon} \left[ \det(\underline{\underline{I}} + \epsilon \underline{\underline{H}}) \hat{\underline{\underline{\delta}}}(\underline{\underline{I}} + \epsilon \underline{\underline{H}}) (\underline{\underline{I}} + \epsilon \underline{\underline{H}})^{-T} \right] \Big|_{\epsilon=0} \\ &= \frac{d}{d\epsilon} [\det(\underline{\underline{I}} + \epsilon \underline{\underline{H}})] \hat{\underline{\underline{\delta}}}(\underline{\underline{I}}) \underline{\underline{I}} \\ &\quad + \det(\underline{\underline{I}}) \frac{d}{d\epsilon} [\hat{\underline{\underline{\delta}}}(\underline{\underline{I}} + \epsilon \underline{\underline{H}})] \Big|_{\epsilon=0} \underline{\underline{I}}^{-T} \\ &\quad + \det(\underline{\underline{I}}) \hat{\underline{\underline{\delta}}}(\underline{\underline{I}}) \frac{d}{d\epsilon} [(\underline{\underline{I}} + \epsilon \underline{\underline{H}})^{-T}] \end{aligned}$$

where  $\det(\underline{\underline{I}}) = 1$  and  $\hat{\underline{\underline{\delta}}}(\underline{\underline{I}}) = \underline{\underline{0}}$  due to stress free initial condition.

$$\Rightarrow \underline{\underline{A}} \underline{\underline{H}} = \frac{d}{d\epsilon} [\hat{\underline{\underline{\delta}}}(\underline{\underline{I}} + \epsilon \underline{\underline{H}})] \Big|_{\epsilon=0} = D\hat{\underline{\underline{\delta}}}(\underline{\underline{I}}) : \underline{\underline{H}} = \underline{\underline{C}} \underline{\underline{H}}$$

so that  $\underline{\underline{A}} = \underline{\underline{C}}$  ✓

An elastic solid with stress free IC has a unique elasticity tensor typically denoted  $\mathbb{C}$  which can be determined from any stress response function  $\hat{\underline{\underline{P}}}(\underline{\underline{F}})$ ,  $\hat{\underline{\underline{\Sigma}}}(\underline{\underline{F}})$  or  $\hat{\underline{\underline{\delta}}}(\underline{\underline{F}})$ .  
 $\Rightarrow$  they have the same linearization at  $\underline{\underline{F}} = \underline{\underline{I}}$

### Balance of angular momentum

$$\hat{\underline{\underline{\delta}}}(\underline{\underline{F}})^T = \hat{\underline{\underline{\delta}}}(\underline{\underline{F}})$$

$$\begin{aligned} [\mathbb{C} \underline{\underline{H}}]^T &= \left( \frac{d}{d\varepsilon} \hat{\underline{\underline{\delta}}}(\underline{\underline{I}} + \alpha \underline{\underline{H}}) \Big|_{\varepsilon=0} \right)^T \\ &= \frac{d}{d\varepsilon} \hat{\underline{\underline{\delta}}}(\underline{\underline{I}} + \alpha \underline{\underline{H}})^T \Big|_{\varepsilon=0} = \frac{d}{d\varepsilon} \hat{\underline{\underline{\delta}}}(\underline{\underline{I}} + \alpha \underline{\underline{H}}) \Big|_{\varepsilon=0} \\ &= \mathbb{C} \underline{\underline{H}} \end{aligned}$$

This implies that  $\mathbb{C}$  has left minor symmetry

$$C_{ijkl} = C_{jikl} \quad \text{or} \quad \underline{\underline{A}} : \mathbb{C} \underline{\underline{B}} = \text{sym}(\underline{\underline{A}}) : \mathbb{C} \underline{\underline{B}}$$

From frame-indifference  $\hat{\underline{\underline{\sigma}}}(\underline{\underline{Q}} \underline{\underline{F}}) = \underline{\underline{Q}} \hat{\underline{\underline{\sigma}}}(\underline{\underline{F}}) \underline{\underline{Q}}^T$   
 and taking  $\underline{\underline{F}} = \underline{\underline{I}}$  and  $\hat{\underline{\underline{\sigma}}}(\underline{\underline{I}}) = \underline{\underline{0}}$  (stress free IC)  
 $\Rightarrow \hat{\underline{\underline{\sigma}}}(\underline{\underline{Q}}) = \underline{\underline{0}}$

Now we use the fact that an infinitesimal rotation can be written as the matrix exponential,  $\exp(\underline{\underline{A}}) = \sum_{j=0}^{\infty} \frac{1}{j!} \underline{\underline{A}}^j = \underline{\underline{I}} + \underline{\underline{A}} + \frac{1}{2} \underline{\underline{A}}^2 + \dots$   
 of a skew tensor  $\underline{\underline{W}} = -\underline{\underline{W}}^T$ .

Here we write  $\underline{\underline{Q}} = \exp(\epsilon \underline{\underline{W}}) \quad \epsilon \in \mathbb{R}$

$$\Rightarrow \hat{\underline{\underline{\sigma}}}(\underline{\underline{Q}}) = \hat{\underline{\underline{\sigma}}}(\exp(\epsilon \underline{\underline{W}})) = \underline{\underline{0}}$$

By definition

$$\begin{aligned} \mathbb{C} \underline{\underline{W}} &= D \hat{\underline{\underline{\sigma}}}(\underline{\underline{I}}) : \underline{\underline{W}} = \frac{d}{d\epsilon} \hat{\underline{\underline{\sigma}}}(\underline{\underline{I}} + \epsilon \underline{\underline{W}}) \Big|_{\epsilon=0} \\ &= \frac{d}{d\epsilon} \hat{\underline{\underline{\sigma}}}(\underline{\underline{I}} + \epsilon \underline{\underline{W}} + \frac{\epsilon^2}{2} \underline{\underline{W}}^2 + \frac{\epsilon^3}{6} \underline{\underline{W}}^3 + \dots) \Big|_{\epsilon=0} \\ &= \frac{d}{d\epsilon} \hat{\underline{\underline{\sigma}}}(\exp(\alpha \underline{\underline{W}})) \Big|_{\epsilon=0} = \underline{\underline{0}} \end{aligned}$$

$$\Rightarrow \mathbb{C} \underline{\underline{W}} = \underline{\underline{0}} \quad \text{for any skew tensor}$$

Therefore  $\mathbb{C} \underline{\underline{H}} = \mathbb{C} \text{sym}(\underline{\underline{H}})$

$\Rightarrow \mathbb{C}$  has right minor symmetry  $C_{ijkl} = C_{ijlk}$

In summary:

- 1) Angular momentum balance:  $C_{ijkl} = C_{jikl}$
- 2) Frame-indifference:  $C_{ijkl} = C_{ijlk}$

## Elasticity Tensors for Isotropic Solid

Let  $\hat{\underline{\underline{\sigma}}}$  be a frame-indifferent Cauchy stress response function for an elastic body with a stress free initial condition. If the body is isotropic the  $\mathbb{C}$  is isotropic (Lecture 21) it takes the form

$$\mathbb{C} \underline{\underline{H}} = \lambda \text{tr}(\underline{\underline{H}}) \underline{\underline{I}} + 2\mu \text{sym}(\underline{\underline{H}}) \quad \lambda, \mu > 0$$

## Linearized Isotropic Elasticity

From the lin. mom. balance

$$\rho_0 \ddot{\underline{u}} = \nabla \cdot (\underline{\mathbb{C}} \nabla \underline{u}) + \rho_0 \underline{b}$$

where the elasticity tensor is given by

$$\underline{\mathbb{C}} \nabla \underline{u} = \lambda \operatorname{tr}(\nabla \underline{u}) \underline{\mathbb{I}} + 2\mu \operatorname{sym}(\nabla \underline{u})$$

$$\begin{aligned} \nabla \cdot [\underline{\mathbb{C}} \nabla \underline{u}] &= \nabla \cdot [\lambda \operatorname{tr}(\nabla \underline{u}) \underline{\mathbb{I}} + 2\mu \operatorname{sym}(\nabla \underline{u})] \\ &= (\lambda u_{k,k} \delta_{ij} + \mu u_{i,j} + \mu u_{j,i}),_{j} \underline{e}_i \\ &= (\lambda u_{k,k,i} + \mu u_{i,jj} + \mu u_{j,ij}) \underline{e}_i \\ &= \lambda \nabla(\nabla \cdot \underline{u}) + \mu \nabla^2 \underline{u} + \mu \nabla(\nabla \cdot \underline{u}) \\ &= (\lambda + \mu) \nabla(\nabla \cdot \underline{u}) + \mu \nabla^2 \underline{u} \end{aligned}$$

substituting into lin. mom. bal.

$$\rho_0 \ddot{\underline{u}} = \mu \nabla^2 \underline{u} + (\lambda + \mu) \nabla(\nabla \cdot \underline{u}) + \rho_0 \underline{b}$$

Navier  
Equation



## General linear elastic solid

Stress response function:

$$\hat{\underline{\underline{P}}}(\underline{\underline{E}}) = \underline{\underline{C}} \underline{\underline{e}} \quad \underline{\underline{e}} = \text{sym}(\nabla \underline{u})$$

Strain energy density

$$W(\underline{\underline{E}}) = \frac{1}{2} \underline{\underline{e}} : \underline{\underline{C}} \underline{\underline{e}}$$

Isotropic model:

$$\underline{\underline{C}} \underline{\underline{e}} = \lambda \text{tr}(\underline{\underline{e}}) \underline{\underline{I}} + 2\mu \underline{\underline{e}}$$

The St. Venant - Kirchhoff model takes this linear model and extends it to large strain by replacing  $\underline{\underline{e}} = \frac{1}{2}(\nabla \underline{u} + \nabla \underline{u}^T)$  with the Green - Lagrange strain tensor  $\underline{\underline{E}} = \frac{1}{2}(\underline{\underline{C}} - \underline{\underline{I}})$ .

Linear:  $\hat{\underline{\underline{\Sigma}}} = \underline{\underline{C}} \underline{\underline{e}} = \lambda \text{tr}(\underline{\underline{e}}) \underline{\underline{I}} + 2\mu \underline{\underline{e}} \quad \underline{\underline{e}} = \nabla \underline{u}$

Non-linear:  $\hat{\underline{\underline{\Sigma}}} = \lambda \text{tr}(\underline{\underline{E}}) \underline{\underline{I}} + 2\mu \underline{\underline{E}} \quad \underline{\underline{E}} = \underline{\underline{C}} - \underline{\underline{I}}$

Note latter cannot be written as a 4<sup>th</sup> order tensor!