

Rate of Deformation Tensors

→ role of deformation gradient in rates

Velocity gradients

Spatial velocity gradient

$$\underline{\underline{L}} = \nabla_{\underline{x}} \underline{v} \quad L_{ij} = \frac{\partial v_i}{\partial x_j}$$

Material velocity gradient

$$\underline{\underline{F}} = \nabla_{\underline{x}} \underline{\varphi} \quad F_{ij} = \varphi_{i,j} \quad \text{and} \quad \underline{V} = \dot{\underline{\varphi}} \quad v_i = \varphi_{i,t}$$
$$\Rightarrow \dot{\underline{\underline{F}}} = \frac{\partial}{\partial t} (\nabla_{\underline{x}} \underline{\varphi}) = \nabla_{\underline{x}} \left(\frac{\partial}{\partial t} \underline{\varphi} \right) = \nabla_{\underline{x}} \underline{V} \quad F_{ij} = V_{i,j}$$

Note analogy

$$\varphi(\underline{x} + \underline{\Delta x}, t) \approx \varphi(\underline{x}, t) + \underline{\underline{F}}(\underline{x}, t) \underline{\Delta x} \quad \underline{\underline{F}} = \nabla \varphi$$

taking material derivative $\dot{\varphi} = v$

$$\underline{V}(\underline{x} + \underline{\Delta x}, t) \approx \underline{V}(\underline{x}, t) + \dot{\underline{\underline{F}}}(\underline{x}, t) \underline{\Delta x} \quad \dot{\underline{\underline{F}}} = \nabla \underline{V}$$

$$\text{Note: } \underline{V}(\underline{x}, t) = \underline{v}(\varphi(\underline{x}, t), t)$$

⇒ same vector field just expressed in \underline{X} or \underline{x}

$$\nabla_{\underline{x}} \underline{V} \neq \nabla_{\underline{x}} \underline{v} |_{\underline{x} = \varphi(\underline{x}, t)}$$

because derivatives are in different directions

To relate $\nabla_{\underline{x}} \underline{v}$ and $\nabla_{\underline{X}} \underline{V}$ use $\underline{V}(\underline{X}, t) = \underline{v}(\underline{\varphi}(\underline{X}, t), t)$

$$\dot{F}_{ij} = \frac{\partial}{\partial X_j} V_i = \frac{\partial}{\partial X_j} v_i(\underline{\varphi}(\underline{X}, t), t)$$

$$\text{where } \frac{\partial}{\partial X_j} = \frac{\partial}{\partial x_k} \frac{\partial x_k}{\partial X_j} = \frac{\partial}{\partial x_k} \varphi_{k,j} = \frac{\partial}{\partial x_k} F_{kj}$$

substituting

$$\begin{aligned} \dot{F}_{ij} &= \frac{\partial}{\partial X_j} v_i(\underline{\varphi}(\underline{X}, t), t) = \frac{\partial}{\partial x_k} v_i(\underline{x}, t) F_{kj} \\ &= v_{i,k} F_{kj} \end{aligned}$$

$$\Rightarrow \underline{\dot{F}} = \nabla_{\underline{x}} \underline{v} \underline{F} = \underline{\underline{\ell}} \underline{F} \quad \text{or} \quad \nabla_{\underline{X}} \underline{V} = \nabla_{\underline{x}} \underline{v} \underline{F}$$

$$\text{also } \underline{\underline{\ell}} = \nabla_{\underline{x}} \underline{v} = \underline{\dot{F}} \underline{F}^{-1} \quad \ell_{ij} = \dot{F}_{ik} F_{kj}^{-1}$$

To understand $\underline{\underline{\ell}}$ we need to decompose it

similar to $\underline{F} = \nabla \varphi$ and $\underline{H} = \nabla \underline{u}$

finite strain: $\underline{F} = \underline{R} \underline{U}$

infinitesimal strain: $\underline{H} = \text{sym}(\underline{H}) + \text{skew}(\underline{H})$

Decomposition of $\underline{\underline{\ell}}$

Split into sym. and skew

$$\underline{\underline{\ell}}(\underline{x}, t) = \underline{\underline{d}}(\underline{x}, t) + \underline{\underline{w}}(\underline{x}, t)$$

$$\underline{\underline{d}} = \frac{1}{2} (\nabla_{\underline{x}} \underline{v} + \nabla_{\underline{x}} \underline{v}^T) \quad \text{rate of strain tensor}$$

$$\underline{\underline{w}} = \frac{1}{2} (\nabla_{\underline{x}} \underline{v} - \nabla_{\underline{x}} \underline{v}^T) \quad \text{spin tensor}$$

Interpretation of $\underline{\underline{d}}$ and $\underline{\underline{\ell}}$

$$\underline{v}(\underline{x} + \Delta \underline{x}, t) \approx \underline{v}(\underline{x}, t) + \nabla_{\underline{x}} \underline{v} \Delta \underline{x} \quad \nabla_{\underline{x}} \underline{v} = \underline{\underline{\ell}} = \underline{\underline{d}} + \underline{\underline{w}}$$

$$\approx \underline{v}(\underline{x}, t) + \underline{\underline{d}} \Delta \underline{x} + \underline{\underline{w}} \Delta \underline{x}$$

because $\underline{\underline{w}}$ is skew \rightarrow axial vector $\underline{\underline{\omega}} = \text{vec}(\underline{\underline{w}})$

$$\text{so that} \quad \underline{\underline{w}} \Delta \underline{x} = \underline{\underline{\omega}} \times \Delta \underline{x}$$

$$\Rightarrow \underline{v}(\underline{x} + \Delta \underline{x}, t) \approx \underline{v}(\underline{x}, t) + \underline{\underline{d}} \Delta \underline{x} + \underline{\underline{\omega}} \times \Delta \underline{x}$$

$\Rightarrow \underline{\underline{d}}$ is rate of change in shape (stretch rate)

$\Rightarrow \underline{\underline{w}}$ is rate of change in orientation (spin)

where $\underline{\underline{\omega}}$ is the angular velocity.

\Rightarrow vorticity: $\nabla_{\underline{x}} \times \underline{v} = 2 \underline{\underline{\omega}} \rightarrow 2$ the spin

Relation of $\underline{\underline{d}}$ to $\underline{\underline{u}}$ and $\underline{\underline{R}}$

$$\underline{\underline{d}} = \dot{\underline{\underline{F}}} \underline{\underline{F}}^{-1}$$

Need material derivatives of $\underline{\underline{F}}^{-1}$ and $\underline{\underline{F}}^{-T}$.

$$\dot{\underline{\underline{I}}} = \frac{d}{dt} (\underline{\underline{F}}^{-1} \underline{\underline{F}}) = \dot{\underline{\underline{F}}}^{-1} \underline{\underline{F}} + \underline{\underline{F}}^{-1} \dot{\underline{\underline{F}}} = \underline{\underline{0}}$$

$$\dot{\underline{\underline{F}}}^{-1} = \underline{\underline{F}}^{-1} \dot{\underline{\underline{F}}} \underline{\underline{F}}^{-1} = \underline{\underline{F}}^{-1} \underline{\underline{d}}$$

$$\dot{\underline{\underline{F}}}^{-T} = (\dot{\underline{\underline{F}}}^{-1})^T = (\underline{\underline{F}}^{-1} \underline{\underline{d}})^T = \underline{\underline{d}} \underline{\underline{F}}^{-T}$$

$$\Rightarrow \boxed{\dot{\underline{\underline{F}}}^{-1} = \underline{\underline{F}}^{-1} \underline{\underline{d}} \quad \dot{\underline{\underline{F}}}^{-T} = \underline{\underline{d}} \underline{\underline{F}}^{-T}}$$

$$\begin{aligned} \underline{\underline{d}} &= \dot{\underline{\underline{F}}} \underline{\underline{F}}^{-1} = \frac{d}{dt} (\underline{\underline{R}} \underline{\underline{U}}) \underline{\underline{F}}^{-1} = (\dot{\underline{\underline{R}}} \underline{\underline{U}} + \underline{\underline{R}} \dot{\underline{\underline{U}}}) \underline{\underline{F}}^{-1} \\ &= (\dot{\underline{\underline{R}}} \underline{\underline{U}} + \underline{\underline{R}} \dot{\underline{\underline{U}}}) (\underline{\underline{R}} \underline{\underline{U}})^{-1} = (\dot{\underline{\underline{R}}} \underline{\underline{U}} + \underline{\underline{R}} \dot{\underline{\underline{U}}}) \underline{\underline{U}}^{-1} \underline{\underline{R}}^T \\ &= \dot{\underline{\underline{R}}} \underline{\underline{U}} \underline{\underline{U}}^{-1} \underline{\underline{R}}^T + \underline{\underline{R}} \dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1} \underline{\underline{R}}^T = \dot{\underline{\underline{R}}} \underline{\underline{R}}^T + \underline{\underline{R}} \dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1} \underline{\underline{R}}^T \end{aligned}$$

show that $\dot{\underline{\underline{R}}} \underline{\underline{R}}^T = -(\dot{\underline{\underline{R}}} \underline{\underline{R}})^T \Rightarrow \text{skew} \left(\frac{d}{dt} (\underline{\underline{R}} \underline{\underline{R}}^T) = \underline{\underline{0}} \right)$

$$\Rightarrow \boxed{\underline{\underline{d}} = \underline{\underline{R}} \text{sym}(\dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1}) \underline{\underline{R}}^T}$$

$$\underline{\underline{w}} = \dot{\underline{\underline{R}}} \underline{\underline{R}}^T + \underline{\underline{R}} \text{skew}(\dot{\underline{\underline{U}}} \underline{\underline{U}}^{-1}) \underline{\underline{R}}^T$$

Shows that $\underline{\underline{d}}$ is not a pure rate of strain

and $\underline{\underline{w}}$ is not a pure rate of rotation

Interpretation of $\underline{\underline{\epsilon}}$ & $\underline{\underline{\omega}}$

By analogy with infinitesimal strain and rotation tensors

Diagonal components of $\underline{\underline{\omega}}$ quantify the instantaneous rate of stretching of line segments at \underline{x} in B_{ϵ} , which are aligned with the coordinate axes.

Similarly, the off-diagonal components of $\underline{\underline{\epsilon}}$ quantify the instantaneous rate of shearing between coord. directions.

The tensor $\underline{\underline{\omega}}$ quantifies the instantaneous rate of rigid rotation at \underline{x} in B_{ϵ} . The axial

vector $\underline{\omega} = \text{vec}(\underline{\underline{\omega}})$ is related to the vorticity

$\underline{\omega} = \nabla_{\underline{x}} \times \underline{v} = 2 \underline{\omega}$. Hence, vorticity measures the rate of rotation or spin at \underline{x} . The vorticity measures twice the angular velocity at \underline{x} .