

Lecture 20: Lagrangian local balance laws

Logistics: HW 7 is due

→ most people have projects Nye
happy to discuss further during
office hours next week

Last time: - Continuum thermodynamics

$$1^{\text{st}} \text{ law: } \rho \dot{u} = -\nabla \cdot \underline{q} + \underline{\underline{\sigma}} : \underline{\underline{\dot{\epsilon}}} + p \underline{\underline{r}}$$

$$\frac{\partial}{\partial t}(\rho u) + \nabla \cdot (\rho u \underline{v} + \underline{q}) = \underline{\underline{\sigma}} : \underline{\underline{\dot{\epsilon}}} + p \underline{\underline{r}}$$

$$2^{\text{nd}} \text{ law: } \rho \dot{s} \geq \frac{p \underline{\underline{r}}}{\theta} - \nabla_x \cdot \left(\frac{\underline{q}}{\theta} \right) \quad \text{Claus. Duham.}$$

⇒ direction of heat conduction

Today: Eulerian (\underline{x}) → Lagrangian (\underline{X})

Summary of Eulerian Balance Laws Equations

mass: $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{v}) = 0$ 1

lin. mom: $\frac{\partial}{\partial t}(\rho \underline{v}) + \nabla \cdot (\rho \underline{v} \otimes \underline{v} - \underline{\underline{\sigma}}) = \rho \underline{b}$ 3

ang. mom: $\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T \quad \sigma_{12} = \sigma_{21} \quad \sigma_{13} = \sigma_{31} \quad \sigma_{23} = \sigma_{32}$ 3

energy: $\frac{\partial}{\partial t}(\rho u) + \nabla \cdot [\rho u \underline{v} + \underline{q}] = \underline{\underline{\sigma}} : \dot{\underline{\underline{\epsilon}}} + \rho r$ 1

Kinematic: $\underline{v}_m = \frac{\partial \varphi}{\partial t}$ 3
11

Unknown fields:

φ	\underline{v}	ρ	$\underline{\underline{\sigma}}$	$\underline{\underline{\epsilon}}$	\underline{q}	u	
3	3	1	9	1	3	1	= 21

We have 21 unknowns but only 11 equations

→ under constrained

Need additional constitutive equations

Remarks:

1) Eulerian formulation the balance laws are independent of φ !

Motion is only needed to determine the shape of the domain.

If B_t is known 8 eqns & 18 unknowns
Need constitutive relations that relate $\underline{\underline{s}}$, q and \underline{u} to ρ , \underline{v} and θ .

Example: $q = -k \nabla \theta$ or $\underline{u} = p \rho(\theta) \theta$

2) Neglecting thermal effects then $\underline{\underline{s}}$, \dot{u} , $\dot{\theta}$ disappear and we have 7 eqns but 12 unknowns
Need constitutive relations that relate

$\underline{\underline{s}}$ to ρ & \underline{v}

Example: Ideal isothermal fluid

$$\underline{\underline{s}} = -p \underline{\underline{I}} \quad \rho = \rho(p) \quad \rho = \rho_0 (1 + \beta (p - p_0))$$

$$\text{mass: } \frac{\partial}{\partial t} \rho(p) + \nabla \cdot (\rho(p) \underline{v}) = 0$$

$$\text{lin. mom.: } \frac{\partial}{\partial t} (\rho \underline{v}) + \nabla \cdot (\rho \underline{v} \otimes \underline{v} + p \underline{I}) = \rho \underline{b}$$

4 unknowns \underline{v} and p and 4 eqns

\Rightarrow closed system

Example: Incompressible Navier-Stokes

$$\rho = \rho_0 \quad \Rightarrow \quad \nabla \cdot \underline{v} = 0 \quad \text{"continuity eqn."}$$

$$\underline{\underline{\sigma}} = -p \underline{I} + \mu (\nabla \underline{v} + \nabla \underline{v}^T)$$

substitute into lin. mom.

$$\frac{\partial}{\partial t} (\rho_0 \underline{v}) + \nabla \cdot [\rho_0 \underline{v} \otimes \underline{v} + p \underline{I} - \mu (\nabla \underline{v} + \nabla \underline{v}^T)] = \rho_0 \underline{b}$$

if $\mu = \text{const.}$

$$\rho_0 \dot{\underline{v}} = \mu \nabla^2 \underline{v} - \nabla p + \rho_0 \underline{b}$$

$$\dot{\underline{v}} = \nu \nabla^2 \underline{v} - \frac{\nabla p}{\rho_0} + \underline{b}$$

$\nu = \frac{\mu}{\rho_0}$
 dynamic viscosity
 kinematic viscosity

Lagrangian balance laws

in terms of \underline{X}

1) By change of variables from Eulerian $\underline{X} = \underline{\varphi}^{-1}(\underline{x}, t)$

2) straight from integral balance laws

→ ~~1~~ to (2)

I Balance of mass

We already did this

$$\rho_m(\underline{X}, t) J(\underline{X}, t) = \rho_0(\underline{X}) \quad J = \det(\underline{F})$$

mass density is known in Lag. formulation

II Balance of linear momentum

Integral balance law

$$\frac{d}{dt} \underline{L}[\Omega_t] = \underline{\tau}[\Omega_t]$$

where $\underline{L}[\Omega_t] = \int_{\Omega_t} \rho(\underline{x}, t) \underline{v}(\underline{x}, t) dV_x$

$$\underline{\tau}[\Omega_t] = \int_{\Omega_t} \rho(\underline{x}, t) \underline{b}(\underline{x}, t) dV_x + \int_{\partial\Omega_t} \underline{\sigma} \underline{n} dA_x$$

change variable from $\underline{x} \rightarrow \underline{X}$

$$\begin{aligned} \underline{L}[\Omega_t] &= \int_{\Omega} \rho_m(\underline{X}, t) \underbrace{\underline{v}_m(\underline{X}, t)}_{\underline{V}(\underline{X}, t) = \dot{\underline{\varphi}}(\underline{X}, t)} J(\underline{X}, t) dV_X \\ &= \int_{\Omega} \rho_0(\underline{X}) \dot{\underline{\varphi}}(\underline{X}, t) dV_X \end{aligned} \quad \rho_0(\underline{X}) = \rho_m J$$

For change of variables on rhs $\underline{\Gamma}_S$ we need

Nanceus formula: $\underline{n} dA_x = J \underline{F}^{-T} \underline{N} dA_X$

$$\begin{aligned} \underline{\Gamma}[\Omega_t] &= \int_{\partial\Omega_t} \underline{\underline{\underline{\sigma}}} \underline{n} dA_x + \int_{\Omega_t} \rho \underline{b} dV_x \\ &= \int_{\partial\Omega} \underline{\underline{\underline{\sigma}}}_m J \underline{F}^{-T} \underline{N} dA_X + \int_{\Omega} \underbrace{\rho_m}_{\rho_0} \underline{b}_m J dV_X \end{aligned}$$

To simplify notation we introduce the tensor

$$\underline{\underline{\underline{P}}}(\underline{X}, t) = J(\underline{X}, t) \underline{\underline{\underline{\sigma}}}_m(\underline{X}, t) \underline{F}(\underline{X}, t)^{-T}$$

first Piola-Kirchhoff stress tensor

$$\underline{\Gamma}[\Omega_t] = \int_{\partial\Omega} \underline{\underline{\underline{P}}} \underline{N} dA_X + \int_{\Omega} \rho_0 \underline{b}_m dV_X$$

substitute into the integral balance law:

$$\frac{d}{dt} \int_{\Omega} \rho_0 \dot{\underline{\varphi}} dV_X = \int_{\partial\Omega} \underline{\underline{P}} \underline{\underline{N}} dA_X + \int_{\Omega} \rho_0 \underline{\underline{b}}_m dV_X$$

since $\Omega \neq \Omega(t)$ and $\rho_0 \neq \rho_0(t)$

$$\int_{\Omega} \rho_0 \ddot{\underline{\varphi}} dV_X = \int_{\Omega} \nabla_X \cdot \underline{\underline{P}} + \rho_0 \underline{\underline{b}}_m dV_X$$

by arbitrary choice of Ω

$$\boxed{\rho_0 \ddot{\underline{\varphi}} = \nabla_X \cdot \underline{\underline{P}} + \rho_0 \underline{\underline{b}}_m} \quad \text{local Lagrangian form of lin. mom. bal.}$$

Note: $\underline{\underline{P}}$ is natural stress tensor in the material description because it relates the traction on a surface to its normal.

spatial:

$$\underline{\underline{t}}(\underline{\underline{x}}, t) = \underline{\underline{s}}(\underline{\underline{x}}, t) \underline{\underline{n}}$$

material:

$$\underline{\underline{T}}(\underline{\underline{X}}, t) = \underline{\underline{P}}(\underline{\underline{X}}, t) \underline{\underline{N}}$$

$\underline{\underline{T}}$ is the (nominal) Piola-Kirchhoff traction vector

$\underline{\underline{t}}$ is the (true) Cauchy traction vector

The resultant force

$$d\underline{f} = \underline{t} dA_x = \underline{T} dA_x$$

$$\underline{t} = \frac{\underline{f}}{A}$$

$$\Rightarrow \underline{T} \parallel \underline{t}$$

III) Balance of angular momentum

Cauchy stress $\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T$

by definition: $\underline{\underline{P}} = J \underline{\underline{\sigma}}_m \underline{\underline{F}}^{-T}$

$$\underline{\underline{\sigma}}_m = \frac{1}{J} \underline{\underline{P}} \underline{\underline{F}}^T = \underline{\underline{\sigma}}_m^T = \left(\frac{1}{J} \underline{\underline{P}} \underline{\underline{F}}^T \right)^T = \frac{1}{J} \underline{\underline{F}} \underline{\underline{P}}^T$$

$$\Rightarrow \underline{\underline{P}} \underline{\underline{F}}^T = \underline{\underline{F}} \underline{\underline{P}}^T$$

$\Rightarrow \underline{\underline{P}} \neq \underline{\underline{P}}^T \Rightarrow \underline{\underline{P}}$ has 9 independent entries

Motivated definition of second Piola-Kirchhoff

stress tensor

$$\underline{\underline{\Sigma}} = \underline{\underline{F}} \underline{\underline{P}}^T$$

$$\underline{\underline{\Sigma}}^T = \underline{\underline{\Sigma}}$$

Networkling in Lagrangian form

$$W[\Omega_t] = \mathcal{P}[\Omega_t] - \frac{d}{dt} K[\Omega_t]$$

From integral balance laws:

$$K[\Omega_t] = \frac{1}{2} \int_{\Omega_t} \rho |\underline{v}|^2 dV_x \quad \leftarrow \int F^{-T} \underline{N} dA_x$$

$$\mathcal{P}[\Omega_t] = \int_{\Omega_t} \rho \underline{b} \cdot \underline{v} dV_x + \int_{\partial\Omega_t} \underline{\underline{\sigma}} \underline{v} \cdot \underline{n} dA_x$$

where we have used $\underline{v} \cdot \underline{\underline{\sigma}} \underline{n} = \underline{\underline{\sigma}}^T \underline{v} \cdot \underline{n} = \underline{\underline{\sigma}} \underline{v} \cdot \underline{n}$

Change in variables

$$K[\Omega_t] = \int_{\Omega} \frac{1}{2} \rho_0 |\dot{\underline{\varphi}}|^2 dV_x$$

$$\mathcal{P}[\Omega_t] = \int_{\Omega} \rho_0 \underline{b}_m \cdot \underline{v}_m dV_x + \int_{\partial\Omega} \int \underline{\underline{\sigma}}_m \underline{v}_m \cdot \underline{F}^{-T} \underline{N} dA_x$$

$$= \int_{\Omega} \rho_0 \underline{b}_m \cdot \underline{v}_m dV_x + \int_{\partial\Omega} \int \underline{\underline{\sigma}}_m \underline{v}_m \cdot \underline{F}^{-T} \underline{N} dA_x$$

$$= \int_{\Omega} \rho_0 \underline{b}_m \cdot \dot{\underline{\varphi}} dV_x + \int_{\partial\Omega} \dot{\underline{\varphi}} \cdot \underline{\underline{P}} \underline{N} dA_x$$

$$\underline{\underline{P}}^T \dot{\underline{\varphi}} \cdot \underline{N}$$

$$\nabla_x \cdot (\underline{\underline{P}}^T \dot{\underline{\varphi}})$$

=

$$= \int_{\Omega} \rho_0 \underline{b}_m \cdot \dot{\underline{\varphi}} + \nabla_x \cdot (\underline{\underline{P}}^T \dot{\underline{\varphi}}) dV_x$$

analogous to Eulerian case

$\dot{\underline{v}}$

$\underline{\underline{\dot{\sigma}}} : \underline{\underline{\dot{\epsilon}}}$ power per unit volume of \mathcal{B}_0

$\underline{\underline{\dot{P}}} : \underline{\underline{\dot{F}}}$ power per unit volume of \mathcal{B}

\Rightarrow see notes $\underline{\underline{Q}} = \int \underline{\underline{F}}^{-1} \underline{\underline{q}}_m$ material heat flux

$$\rho_0 \dot{u} = \underline{\underline{P}} : \underline{\underline{\dot{F}}} - \nabla_x \cdot \underline{\underline{Q}} + \rho_0 R$$

local Lagrangian energy balance

$$R = r_m \quad u = u_m$$

ship

Lagrangian balance laws

Kinematic: $\underline{\underline{V}} = \underline{\underline{\dot{\Phi}}}$ 3

lin. mom.: $\rho_0 \underline{\underline{\dot{V}}} = \nabla_x \cdot \underline{\underline{P}} + \rho_0 \underline{\underline{b}}_m$ 3

ang mom.: $\underline{\underline{P}} \underline{\underline{F}}^T = \underline{\underline{F}} \underline{\underline{P}}^T$ 3

energy: $\rho_0 \dot{u} = \underline{\underline{P}} : \underline{\underline{\dot{F}}} - \nabla_x \cdot \underline{\underline{Q}} + \rho_0 R$ 1

Lagrangian fields:

φ \underline{V} \underline{P} \oplus \underline{Q} U

$$3 \quad 3 \quad 9 \quad 1 \quad 3 \quad 1 \quad = 20$$

\Rightarrow 20 unknown & 10 eqns.

Notes:

1) In many situations \underline{V} is not needed
 \Rightarrow 17 ^{unknowns} eqns & 7 eqns

2) Constitutive relations that relate

$\underline{\Sigma}$ to φ

$\underline{Q}, \underline{U}$ to \oplus

3) Isothermal system $\underline{\Sigma} = \underline{\Sigma}(\varphi)$