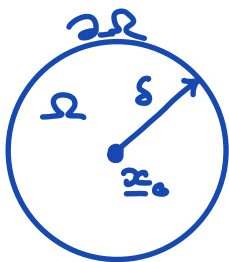


Cauchy Stress Tensor

Force balance in limit of small body.



$V_\Omega = \text{volume}$

$A_{\partial\Omega} = \text{surf. area}$

$$\lim_{\delta \rightarrow 0} \underline{f} = m \underline{g}$$

$$m = \int_{\Omega} \rho \, dV$$

$$\underline{f} = \underline{f}_b[\Omega] + \underline{f}_s[\partial\Omega]$$

$$= \int_{\Omega} \underline{b} \, dV + \oint_{\partial\Omega} \underline{t} \, dS$$

$$\lim_{\delta \rightarrow 0} m = \int_{\Omega} \rho(\underline{x}) \, dV \approx \rho(\underline{x}_0) \int_{\Omega} dV = \rho_0 V_\Omega$$

$$\lim_{\delta \rightarrow 0} \underline{f}_b[\Omega] = \int_{\Omega} \underline{b} \, dV \approx \underline{b}(\underline{x}_0) \int_{\Omega} dV = \underline{b}_0 V_\Omega$$

substitute into 2nd law

$$\lim_{\delta \rightarrow 0} \oint_{\partial\Omega} \underline{t} \, dA = \int_{\Omega} \rho \underline{g} - \underline{b} \, dV \approx (\rho \underline{g} - \underline{b}) V_\Omega$$

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\partial\Omega}} \oint_{\partial\Omega} \underline{t} \, dA = \frac{V_\Omega}{A_{\partial\Omega}} (\rho \underline{g} - \underline{b})$$

Volume vanishes faster than surface area!

$$\lim_{\delta \rightarrow 0} \frac{V_{\Omega}}{A_{\partial\Omega}} = 0$$

Consider a sphere: $V_{\Omega} = \frac{4}{3} \pi \delta^3$ $A_{\partial\Omega} = 4 \pi \delta^2$

$$\lim_{\delta \rightarrow 0} \frac{V_{\Omega}}{A_{\partial\Omega}} = \frac{\delta}{3} = 0$$

But this holds for any shape.

HW: Show $\frac{V}{A} \rightarrow 0$ for tetrahedron

Surface forces vanish of infinitesimal body

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\Omega}} \oint_{\partial\Omega} \underline{t} \, dA = 0$$

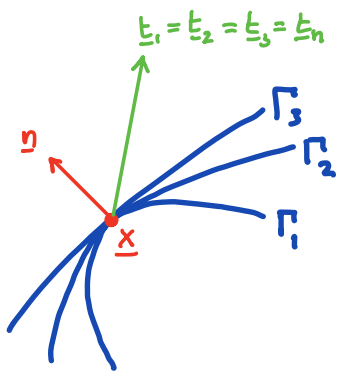
Note: • $\frac{1}{A_{\Omega}}$ normalization

• assume ρ , $|\underline{g}|$ and $|\underline{a}|$ are finite

\Rightarrow basis for derivation of Cauchy stress tensor.

Cauchy's postulate

The traction field \underline{t}_n on a surface Γ in \mathcal{B} depends only pointwise on the unit normal field \underline{n} . In particular, there is a traction function such that $\underline{t}_n = \underline{t}_n(\underline{n}(\underline{x}), \underline{x})$.



This assumes that the traction field is independent of $\nabla \underline{n}$ and hence the curvature

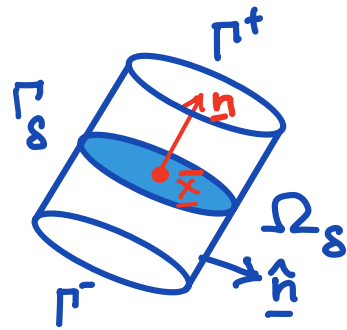
of the surface. Therefore the traction \underline{t}_i on the set of surfaces Γ_i that are tangent at \underline{x} is the same, $\underline{t}_i = \underline{t}_n$.

Law of Action and Reaction

If the traction field, $\underline{t}(\underline{n}, \underline{x})$, is continuous and bounded, then

$$\underline{t}(-\underline{n}, \underline{x}) = -\underline{t}(\underline{n}, \underline{x})$$

for all \underline{n} and $\underline{x} \in B$.



Disk D centered on \underline{x}

Cylinder Ω_δ center \underline{x} axis \underline{n} .

Faces: Γ^+ , Γ^- , Γ_δ

outward normal $\hat{\underline{n}}$ on $\partial\Omega_\delta = \underbrace{\Gamma^+ \cup \Gamma^- \cup \Gamma_\delta}_{\text{union}}$

Note: on Γ^+ $\hat{\underline{n}} = \underline{n}$ and on Γ^- $\hat{\underline{n}} = -\underline{n}$

$\delta \rightarrow 0$: $\Gamma^\pm \rightarrow D$ and $\Gamma_\delta \rightarrow 0$

Resultant surface force

$$\underline{\Gamma}_s[\partial\Omega_s] = \int_{\partial\Omega_s} \underline{t}_n(\underline{n}, \underline{x}) dA$$

since $2\Omega_s = \Gamma_s \cup \Gamma^+ \cup \Gamma^-$

$$\underline{\Gamma}_s[\partial\Omega_s] = \int_{\Gamma_s} \underline{t}(\hat{\underline{n}}, \underline{x}) dA + \int_{\Gamma^+} \underline{t}(\underline{n}, \underline{x}) dA + \int_{\Gamma^-} \underline{t}(-\underline{n}, \underline{x}) dA$$

$$\lim_{s \rightarrow 0} \left[\int_{\Gamma_s} \underline{t}(\hat{\underline{n}}(\underline{x}), \underline{x}) dA + \int_{\Gamma^+} \underline{t}(\underline{n}, \underline{x}) dA + \int_{\Gamma^-} \underline{t}(-\underline{n}, \underline{x}) dA \right] = 0$$

the first term vanishes because \underline{t} is bounded and

$\Gamma_s \rightarrow 0$. Using the fact that $\Gamma^\pm \rightarrow D$ we have in the limit

$$\int_D \underline{t}(\underline{n}, \underline{y}) + \underline{t}(-\underline{n}, \underline{y}) dA = 0$$

since the radius of D is arbitrary the integrand

must vanish so that $\underline{t}(\underline{n}, \underline{x}) + \underline{t}(-\underline{n}, \underline{x}) = 0$ ✓

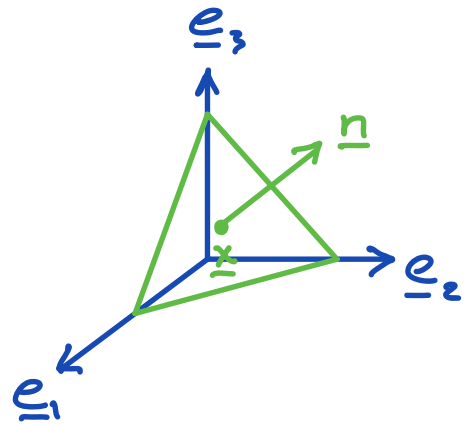
The Stress tensor

Cauchy's Theorem

Let $\underline{t}(\underline{n}, \underline{x})$ be the traction field for body B that satisfies Cauchy's postulate. Then $\underline{t}(\underline{n}, \underline{x})$ is linear in \underline{n} , that is, for each $\underline{x} \in B$ there is a second-order tensor field $\underline{\underline{\sigma}}(\underline{x}) \in V^2$ such that $\underline{t}(\underline{n}, \underline{x}) = \underline{\underline{\sigma}}(\underline{x}) \underline{n}$ called the Cauchy stress field for B .

To establish this consider a frame $\{\underline{e}_i\}$, a point $\underline{x} \in B$ and a normal \underline{n} s.t. $\underline{n} \cdot \underline{e}_i > 0$.

For $\delta > 0$, let Γ_δ denote a triangular region with center \underline{x} , normal \underline{n} and maximum edge length δ .



Let Ω_δ be the tetrahedron bounded by Γ_δ and the three coordinate planes. These planes form three faces Γ_j with outward normals $\underline{n}_j = -\underline{e}_j$. The volume of Ω_δ goes to zero as δ becomes small.

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\partial\Omega_\delta}} \int_{\partial\Omega_\delta} \underline{t}(\underline{n}(\underline{x}), \underline{y}) dA = 0$$

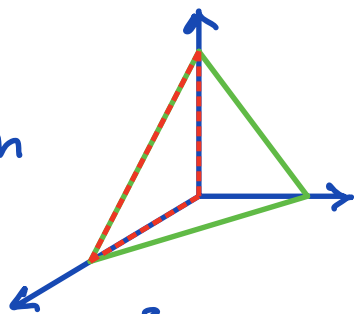
Where $A_{\partial\Omega_\delta}$ is the surface area of Ω_δ .
 Since $\partial\Omega_\delta = \Gamma_\delta \cup \Gamma_1 \cup \Gamma_2 \cup \Gamma_3$ we have

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\partial\Omega_\delta}} \left[\int_{\Gamma_\delta} \underline{t}(\underline{n}, \underline{y}) dA + \sum_{j=1}^3 \int_{\Gamma_j} \underline{t}(-\underline{e}_j, \underline{y}) dA \right] = 0$$

Since each face Γ_j can be linearly mapped onto Γ_δ with constant Jacobian

$$n_j = \underline{n} \cdot \underline{e}_j > 0 \text{ so that } A_{\Gamma_j} = n_j A_{\Gamma_\delta}$$

$$\Rightarrow A_{\partial\Omega_\delta} = A_{\Gamma_\delta} + \sum_{j=1}^3 A_{\Gamma_j} = \lambda A_{\Gamma_\delta} \quad \lambda = 1 + \sum_{j=1}^3 n_j$$



substituting we obtain

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\partial \Omega_\delta}} \left[\int_{\Gamma_\delta} \underline{t}(\underline{n}, \underline{x}) dA + \sum_{j=1}^3 \int_{\delta} \underline{t}_n(-\underline{e}_j, \underline{y}) n_j dA \right] = 0$$

$$\lim_{\delta \rightarrow 0} \frac{1}{\lambda A_{\Gamma_\delta}} \int_{\Gamma_\delta} \underline{t}(\underline{n}, \underline{y}) + \sum_{j=1}^3 \underline{t}(-\underline{e}_j, \underline{y}) n_j dA = 0$$

As $\delta \rightarrow 0$ the area Γ_δ shrinks to \underline{x} so that by the mean value theorem for integrals the limit is given by the integrand. Hence

$$\underline{t}(\underline{n}, \underline{x}) + \sum_{j=1}^3 \underline{t}(-\underline{e}_j, \underline{x}) n_j = 0$$

Using the Law of Action and Reaction

$$\underline{t}(\underline{n}, \underline{x}) = - \sum_{j=1}^3 \underline{t}(\underline{e}_j, \underline{x}) n_j = \sum_{j=1}^3 \underline{t}(\underline{e}_j, \underline{x}) n_j$$

or with summation convention

$$\underline{t}(\underline{n}, \underline{x}) = \underline{t}(\underline{e}_j, \underline{x}) n_j$$

using the definition of dyadic product

$$(\underline{t}(\underline{e}_j, \underline{x}) \otimes \underline{e}_j) \underline{n} = \underbrace{(\underline{e}_j \cdot \underline{n})}_{n_i \underline{e}_j \cdot \underline{e}_i = n_i \delta_{ij} = n_j} \underline{t}(\underline{e}_j, \underline{x})$$

So that we have

$$\underline{t}(\underline{n}, \underline{x}) = (\underline{t}(\underline{e}_j, \underline{x}) \otimes \underline{e}_j) \underline{n} = \underline{\underline{\sigma}} \underline{n}$$

$$\underline{\underline{\sigma}} = \underline{t}(\underline{e}_j, \underline{x}) \otimes \underline{e}_j$$

substituting $\underline{t}(\underline{e}_j, \underline{x}) = t_i(\underline{e}_j, \underline{x}) \underline{e}_i$ we obtain the definition of the Cauchy stress tensor

$$\underline{\underline{\sigma}} = \sigma_{ij} \underline{e}_i \otimes \underline{e}_j \quad \text{with} \quad \sigma_{ij} = t_i(\underline{e}_j, \underline{x})$$

Hence σ_{ij} is the i -th component of the traction on the j -th coordinate plane.

The traction vectors on

the coord. planes at \underline{x} are

$$\underline{t}(\underline{e}_1, \underline{x}) = t_i(\underline{e}_1, \underline{x}) \underline{e}_i = \sigma_{i1}(\underline{x}) \underline{e}_i$$

$$\underline{t}(\underline{e}_2, \underline{x}) = t_i(\underline{e}_2, \underline{x}) \underline{e}_i = \sigma_{i2}(\underline{x}) \underline{e}_i$$

$$\underline{t}(\underline{e}_3, \underline{x}) = t_i(\underline{e}_3, \underline{x}) \underline{e}_i = \sigma_{i3}(\underline{x}) \underline{e}_i$$

