

Lecture 26: Creeping Flow - Stokes Eqn.

Logistics: - HW 7 graded

Q2: Rigid rotation about fixed point \underline{Y}

$$\varphi = \underline{Y} + \Omega (\underline{X} - \underline{Y})$$

$$\underline{F} = \nabla \varphi = \frac{\partial \varphi_i}{\partial x_j} \underline{e}_i \otimes \underline{e}_j = \underline{\Omega}$$

$$\underline{C} = \underline{F}^T \underline{F} = \underline{\Omega}^T \underline{\Omega} = \underline{I}$$

- HW 8 Thursday (11/30) last chance!

- Course Evaluations

Last time: - Navier-Stokes Equations

Newtonian Stress: $\underline{\sigma} = -p \underline{I} + \eta (\nabla \underline{v} + \nabla \underline{v}^T)$

$$\rho_0 \left[\frac{\partial \underline{\sigma}}{\partial t} + (\nabla \underline{v}) \underline{\sigma} \right] = \eta \nabla^2 \underline{v} - \nabla p + \rho_0 \underline{g}$$

- Decay of kinetic Energy

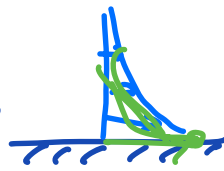
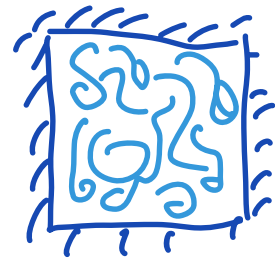
$$k(t) \leq k_0 e^{-\frac{\eta}{\lambda \rho_0} t}$$

- Rayleigh's problem

$$u(y, t) = U \left(1 - \operatorname{erf} \left(\frac{y}{\sqrt{4\nu t}} \right) \right)$$

$\frac{L^2}{T}$

$$\nu = \frac{\eta}{\rho_0} \text{ mom. diffusivity}$$



Today: - Creeping flows

\underline{u}

Scaling of N-S equations

$$\rho \frac{\partial \underline{v}}{\partial t} + (\nabla \underline{v}) \underline{v} = \gamma \nabla^2 \underline{v} - \nabla p + \rho \underline{g}$$

introduce reduced pressure:

$$-\nabla p + \rho \underline{g} = -(\nabla p + \rho g \hat{z}) = -\nabla \underbrace{(p + \rho g z)}_{\pi} = -\nabla \pi$$

so we have

$$\rho \left[\frac{\partial \underline{v}}{\partial t} + (\nabla \underline{v}) \underline{v} \right] = \gamma \nabla^2 \underline{v} - \nabla \pi$$

$\nabla \cdot \underline{v} = 0$

Non-dimensionalize with generic quantities to define standard dimensionless parameters:

- Dependent variable: \underline{v}, π
- Independent variables: \underline{x}, t
- Parameters: $\rho \left[\frac{M}{L^3} \right] \quad \gamma \left[\frac{M}{LT} \right] \rightarrow \nu = \frac{\gamma}{\rho} \left[\frac{L^2}{T} \right]$
+ Geometry, BC, IC

Use parameter combinations to scale variable:

$$\underline{v}' = \frac{\underline{v}}{V_c} \quad \pi' = \frac{\pi}{\pi_c} \quad \underline{x}' = \frac{\underline{x}}{x_c} \quad t' = \frac{t}{t_c}$$

⇒ substitute into governing equations

$$\rho \frac{\partial \underline{u}}{\partial t} = \rho \frac{\partial (\underline{u}_c \underline{u}')}{\partial (t_c t')} = \frac{\rho \underline{u}_c}{t_c} \frac{\partial \underline{u}'}{\partial t'}$$

$$\frac{\rho \underline{u}_c}{t_c} \frac{\partial \underline{u}'}{\partial t'} + \frac{\rho \underline{u}_c^2}{x_c} (\nabla' \underline{u}') \underline{u}' = \frac{\eta \underline{u}_c}{x_c^2} \nabla'^2 \underline{u}' - \frac{\pi_c}{x_c} \nabla' \pi'$$

Option 1: Scale to accumulation term

$$1 \frac{\partial \underline{u}'}{\partial t'} + \underbrace{\frac{\underline{u}_c t_c}{x_c}}_{\Pi_1} \underbrace{\frac{t_c}{t_A}}_{\Pi_2} (\nabla' \underline{u}') \underline{u}' = \underbrace{\frac{\eta t_c}{x_c^2}}_{\Pi_2=1} \nabla'^2 \underline{u}' - \underbrace{\frac{\pi_c t_c}{x_c \rho \underline{u}_c}}_{\Pi_3=1} \nabla' \pi'$$

$\nu = \frac{\eta}{\rho}$ inertial

Three dimensionless groups: \Rightarrow define time scales

$$\Pi_1 = \frac{\underline{u}_c t_c}{x_c} = 1 \Rightarrow \text{advective time scale: } t_c = t_A = \frac{x_c}{\underline{u}_c}$$

$$\Pi_2 = \frac{\nu t_c}{x_c^2} = 1 \Rightarrow \text{diffusive time scale: } t_c = t_D = \frac{x_c^2}{\nu}$$

Use Π_3 to define pressure scale

$$\Pi_3 = \frac{\pi_c t_c}{x_c \rho \underline{u}_c} = 1 \Rightarrow \underline{\pi}_c = \frac{x_c \rho \underline{u}_c}{t_c}$$

Choose a diffusive time scale: $t_c = t_D = \frac{x_c^2}{\nu}$

$$\Rightarrow \frac{\partial \underline{u}'}{\partial t'} + \underbrace{\frac{b_D}{t_A}}_{\Pi_1 = \frac{\underline{u}_c x_c}{\nu}} (\nabla' \underline{u}') \underline{u}' = \nabla'^2 \underline{u}' - \nabla' \pi'$$

⇒ only one remaining dim. less group.

Reynolds number: $Re = \frac{v_c x_c}{\nu} = \frac{t_D}{t_A}$

⇒ Peclet number for lin. momentum

Hence we have dropping the primes

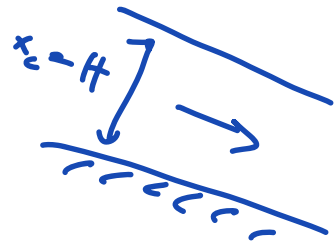
$$\frac{\partial \underline{v}}{\partial t} + Re (\nabla \underline{v}) \underline{v} = \nabla^2 \underline{v} - \nabla \pi$$

as $Re \rightarrow 0$ advective momentum transfer vanishes

Re for a glacier

$$\rho \sim 10^3 \frac{\text{kg}}{\text{m}^3} \quad v_c \sim 10^2 \frac{\text{m}}{\text{yr}} \sim 10^{-6} \frac{\text{m}}{\text{s}}$$

$$\eta \sim 10^{14} \text{ Pa s} \quad x_c \sim 10^2 \text{ m}$$



$$Re = \frac{v_c x_c \rho}{\eta} = \frac{10^{-6+2+3}}{10^{14}} = 10^{-1-14} = 10^{-15} \ll 1$$

$$\Rightarrow \frac{\partial \underline{v}}{\partial t} = \nabla^2 \underline{v} - \nabla \pi \quad \text{linear, transient}$$

Is it worth resolving the transient?

$$\tau_p = \frac{x_c^2 \rho}{\eta} = 10^{4+3-14} \text{ s} = \underline{10^{-7} \text{ s}}$$

much smaller than glacial time scales

Option 2: Scale to non. diffusion tensor

$$\frac{\rho \sigma_c}{t_c} \frac{\partial \underline{u}'}{\partial t'} + \frac{\rho \sigma_c^2}{x_c} (\nabla' \underline{u}') \underline{u}' = \frac{\eta v_c}{x_c^2} \nabla'^2 \underline{u}' - \frac{\pi_c}{x_c} \nabla' \pi'$$

divide by $\frac{\eta v_c}{x_c^2}$

$$\frac{x_c^2}{\rho t_c} \frac{\partial \underline{u}'}{\partial t'} + \frac{v_c x_c}{\nu} (\nabla' \underline{u}') \underline{u}' = \nabla'^2 \underline{u}' - \frac{\pi_c x_c}{\eta v_c} \nabla' \pi'$$

$\frac{x_c^2}{\rho t_c} = \frac{\eta}{\rho}$

$$\hookrightarrow \pi_c = \frac{\eta \sigma_c}{x_c}$$

choose a time scale: $t_c = t_A = \frac{x_c}{v_c}$

$$\text{Re} \left(\frac{\partial \underline{u}'}{\partial t'} + (\nabla' \underline{u}') \underline{u}' \right) = \nabla'^2 \underline{u}' - \nabla' \pi'$$

$$\frac{v_c x_c}{\nu} \sim 10^{-15}$$

⇒ Stokes Equation

$$\boxed{\begin{aligned} \nabla'^2 \underline{u}' &= \nabla' \pi \\ \nabla' \cdot \underline{u}' &= 0 \end{aligned}}$$

dimensionless

$$\mu = \eta$$

Redimensionalize: $\underline{u}' = \frac{\underline{u}}{v_c}$ $\pi'' = \frac{\pi}{\frac{\eta x_c}{v_c}}$ $\underline{x}' = \frac{\underline{x}}{x_c}$

$$\frac{x_c^2}{\eta} \nabla'^2 \underline{u}' = \frac{x_c^2}{\eta v_c} \nabla' \pi$$

$$\boxed{\begin{aligned} \eta \nabla^2 \underline{u} &= \nabla \pi \\ \nabla \cdot \underline{u} &= 0 \end{aligned}}$$

dimensional

Stokes equation

This is assuming $y = \text{const.}$

Properties of Stokes:

1) Linearity

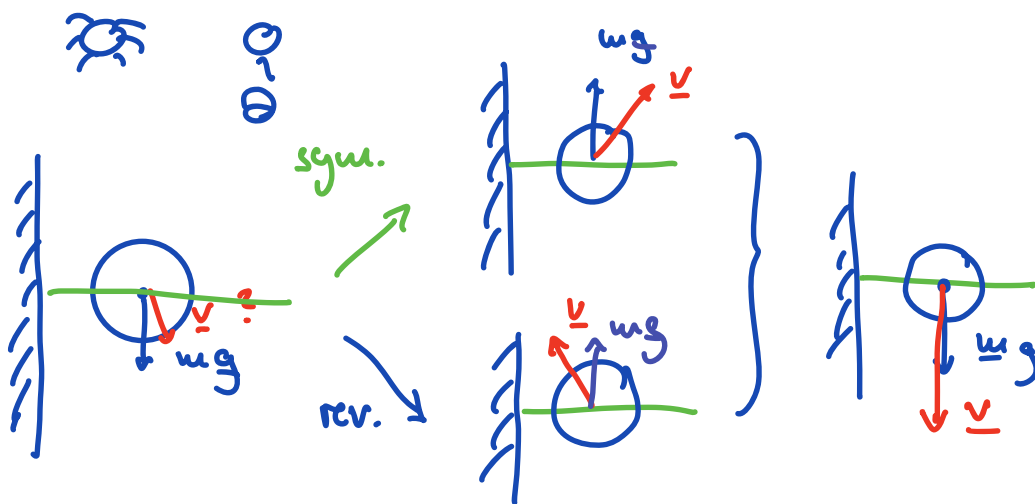
→ Construct solutions by lin. superposition

2) Instantaneous

no time dependence other than that introduced by boundary conditions.

3) Reversibility

If body force and velocity on boundary are reversed so is the velocity everywhere.



In Earth Science most creeping flows are variable viscosity!

$$\rho \frac{\partial \underline{u}}{\partial t} + (\nabla \underline{u}) \underline{u} = \nabla \cdot \underline{\underline{\sigma}} + \rho \underline{g}$$

$$\underline{\underline{\sigma}} = -p \underline{\underline{I}} + \eta (\nabla \underline{u} + \nabla \underline{u}^T)$$

$$\nabla \cdot \underline{\underline{\sigma}} = -\nabla p + \nabla \cdot [\eta (\nabla \underline{u} + \nabla \underline{u}^T)]$$

$$\rho \frac{\partial \underline{u}}{\partial t} + (\nabla \underline{u}) \underline{u} = \underbrace{\nabla \cdot [\eta (\nabla \underline{u} + \nabla \underline{u}^T)]}_{\eta \nabla^2 \underline{u}} - \nabla \pi$$

same scaling as option 2: $\eta \neq \text{const.}$
 $\eta' = \frac{\eta}{\eta_c}$

$$\text{Re} \left(\frac{\partial \underline{u}'}{\partial t} + (\nabla \underline{u}') \underline{u}' \right) = \nabla \cdot [\eta' (\nabla \underline{u}' + \nabla \underline{u}'^T)] - \nabla \cdot \pi'$$

$\text{Re} \sim 10^{-15}$

Variable viscosity Stokes equation:

$$\nabla \cdot [\eta (\nabla \underline{u} + \nabla \underline{u}^T)] = \nabla \pi$$

$$\nabla \cdot \underline{\underline{\sigma}} = 0$$

Two common sources of viscosity variation:

1) $\eta = \eta(T)$ temperature dependence

2) $\eta = \eta(\underline{\sigma})$ non-Newtonian fluids

→ power law creep

