

Lecture 5: Cauchy Stress Tensor

Logistics: - HWI due Thurs. at 9th am

- Office hours 4-5 pm today on zoom

Last time: - Second-order Tensors

$$\underline{\underline{v}} = \underline{\underline{A}} \underline{\underline{u}}$$

- Dyadic product: $(\underline{\underline{a}} \otimes \underline{\underline{b}}) \underline{\underline{v}} = (\underline{\underline{b}} \cdot \underline{\underline{v}}) \underline{\underline{a}}$

- Tensor basis: $\underline{\underline{S}} = \sum_{i,j} S_{ij} \underline{\underline{e}_i} \otimes \underline{\underline{e}_j}$
 $S_{ij} = \underline{\underline{e}_i} \cdot \underline{\underline{S}} \underline{\underline{e}_j}$

$$[\underline{\underline{a}} \otimes \underline{\underline{b}}] = \begin{bmatrix} a_1 b_1 & a_1 b_2 & a_1 b_3 \\ a_2 b_1 & a_2 b_2 & a_2 b_3 \\ a_3 b_1 & a_3 b_2 & a_3 b_3 \end{bmatrix} \quad \underline{\underline{A}} \underline{\underline{B}} = \underline{\underline{H}}$$

- Tensor algebra: $\underline{\underline{\alpha}}(\underline{\underline{A}} + \underline{\underline{B}})\underline{\underline{b}} = \underline{\underline{\alpha A}} \underline{\underline{b}} + \underline{\underline{\alpha B}} \underline{\underline{b}}$

- Tensor properties: Transpose, trace

Today: - Cauchy stress tensor

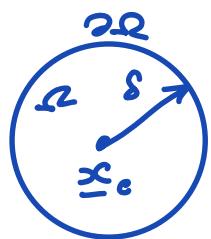
- Cauchy's postulate

- Achian - Reaching

- Cauchy's Theorem

Cauchy - Stress Tensor

Force balance are in limit of small body



$$\lim_{\delta \rightarrow 0} f = m g$$

$$m = \int_{\Omega} \rho dV$$

$$V_{\Omega} = \text{Volume} \quad f = \Gamma_b [\Omega] + \Gamma_s [\partial\Omega]$$

$$A_{\Omega} = \text{surf. area} \quad = \int_{\Omega} \rho g dV + \oint_{\partial\Omega} \underline{\underline{f}} \cdot \underline{\underline{n}} dS$$

$$\lim_{\delta \rightarrow 0} m = \int_{\Omega} \rho(x) dV \approx \rho(x_0) \int_{\Omega} dV = \rho_0 V_{\Omega}$$

$$\lim_{\delta \rightarrow 0} \Gamma_b [\Omega] = \int_{\Omega} \rho g dV \approx \rho_0 g_0 V_{\Omega}$$

$$\text{Substituting} \quad \Gamma_s [\partial\Omega] = m g - \Gamma_b [\Omega]$$

$$\lim_{\delta \rightarrow 0} \oint_{\partial\Omega} \underline{\underline{f}} \cdot \underline{\underline{n}} dA = \int_{\Omega} \rho g dV \approx \rho_0 (g_0 - g_0) V_{\Omega}$$

distributing are

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{\Omega}} \oint_{\partial\Omega} \underline{\underline{f}} \cdot \underline{\underline{n}} dA = \underline{\underline{\rho_0}} \underline{\underline{(g_0 - g_0)}}$$

Volume vanishes faster than surface area

$$\lim_{\delta \rightarrow 0} \frac{V_\Omega}{A_\Omega} = 0$$

Consider sphere: $V_\Omega = \frac{4}{3} \pi \delta^3$ $A_\Omega = 4\pi \delta^2$

$$\lim_{\delta \rightarrow 0} \frac{V_\Omega}{A_\Omega} = \frac{\frac{4}{3} \pi \delta^3}{4\pi \delta^2} = 0$$

\Rightarrow This also holds for other bodies
all

Force balance on infinitesimal body

$$\boxed{\lim_{\delta \rightarrow 0} \frac{1}{A_\Omega} \oint \underline{\tau} dA = 0}$$

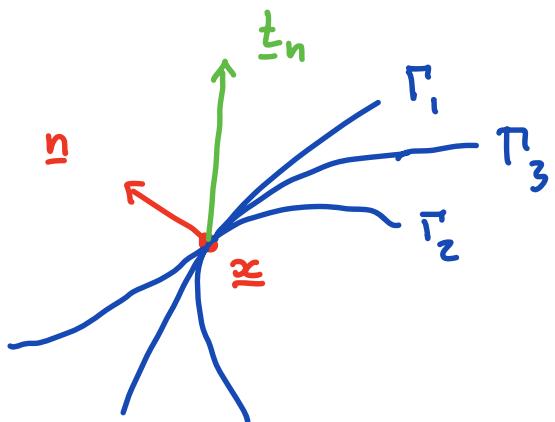
Note: • $\frac{1}{A_\Omega}$ normalization

- assumed $\rho, (\underline{g}), (\underline{\tau}), (\underline{t})$
are all finite and continuous

\Rightarrow basis for derivation of Cauchy-Stress tensor

Cauchy's postulate

The traction field, \underline{t}_n on surface Γ depends only pointwise on the unit normal vector \underline{n} . In particular there is a traction field st. $\boxed{\underline{t}_n = \underline{t}_n(\underline{n}, \underline{x})}$



$\Rightarrow \underline{t}_n$ is independent of $\nabla \underline{n}$ and hence the curvature of surface.

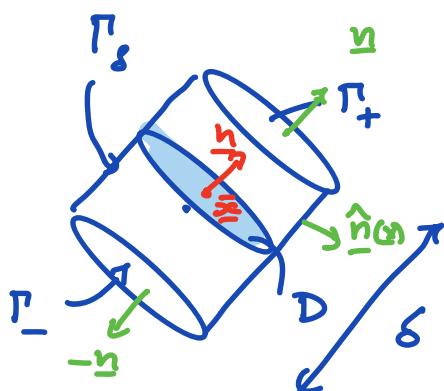
Law of Action-Reaction

If \underline{t}_n is continuous & bounded

$$\boxed{\underline{t}_n(-\underline{n}, \underline{x}) = -\underline{t}_n(\underline{n}, \underline{x})}$$

Disk of area D

$$\partial D = \Gamma^+ \cup \Gamma^- \cup \Gamma_s$$



resultant surface force:

$$\underline{\underline{\sigma}}[\underline{\underline{\sigma}}] = \int_{\partial\Omega} \underline{\underline{t}}_n(\underline{n}, \underline{\underline{\sigma}}) dA$$

$$= \int_{\Gamma_s} \underline{\underline{t}}_n(\underline{n}(\underline{\underline{\sigma}}), \underline{\underline{\sigma}}) dA + \int_{\Gamma_+} \underline{\underline{t}}_n(\underline{n}, \underline{\underline{\sigma}}) dA + \int_{\Gamma_-} \underline{\underline{t}}_n(-\underline{n}, \underline{\underline{\sigma}}) dA$$

$$\lim_{\delta \rightarrow 0} \frac{1}{A_\delta} \underline{\underline{\sigma}}[\underline{\underline{\sigma}}] = \frac{1}{A} \int_D \underline{\underline{t}}_n(\underline{n}, \underline{\underline{\sigma}}) + \underline{\underline{t}}_n(-\underline{n}, \underline{\underline{\sigma}}) dA = C$$

localization: Because the location & radius of disk are arbitrary \Rightarrow integrand must be zero everywhere.

$$\Rightarrow \underline{\underline{t}}_n(\underline{n}, \underline{\underline{\sigma}}) + \underline{\underline{t}}_n(-\underline{n}, \underline{\underline{\sigma}}) = 0$$

$$\underline{\underline{t}}_n(-\underline{n}, \underline{\underline{\sigma}}) = -\underline{\underline{t}}_n(\underline{n}, \underline{\underline{\sigma}}) \quad \checkmark$$

Cauchy's Theorem

Let $\underline{\underline{t}}(\underline{n}, \underline{\underline{\sigma}})$ satisfy Cauchy's postulate. Then $\underline{\underline{t}}(\underline{n}, \underline{\underline{\sigma}})$ is linear in \underline{n} , that is, for each $\underline{\underline{\sigma}}$ there is a second-order tensor field $\underline{\underline{\Theta}}(\underline{\underline{\sigma}}) \in \mathcal{V}^c$

such that

$$\underline{\underline{t}}(\underline{n}, \underline{\underline{\sigma}}) = \underline{\underline{\Theta}}(\underline{\underline{\sigma}}) \underline{n}$$

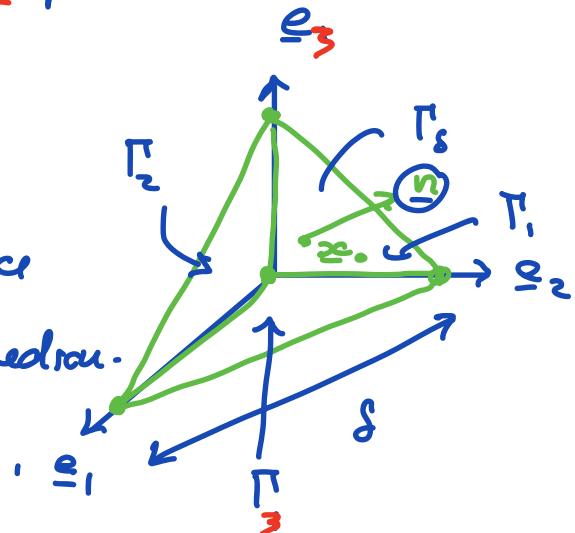
called the Cauchy stress field.

$$\{\underline{\epsilon}_i\}$$

$\underline{\epsilon}_i$ and \underline{n} define a surface

that defines a irregular tetrahedron.

s length of max side



Surface area: $2\Omega = \Gamma_s \cup \Gamma_1 \cup \Gamma_2 \cup \Gamma_3$

↑ normal on Γ_i is $\underline{n}_i = -\underline{\epsilon}_i$
outward

Force balance on Ω in limit of $s \rightarrow 0$

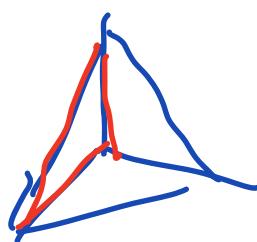
$$\lim_{s \rightarrow 0} \frac{1}{A_\Omega} \left[\oint_{\Gamma_s} \underline{\epsilon}(\underline{n}, \underline{\epsilon}) dA + \sum_{j=1}^3 \oint_{\Gamma_j} \underline{\epsilon}(-\underline{\epsilon}_j, \underline{\epsilon}) dA \right] = 0$$

Note: $n_j = \underline{n} \cdot \underline{\epsilon}_j \geq 0$

$$A_{\Gamma_j} = n_j A_{\Gamma_s}$$

\Rightarrow future HW's

$$A_{2\Omega} = A_{\Gamma_s} + \sum_{j=1}^3 A_{\Gamma_j} = \lambda A_{\Gamma_s} \quad \lambda = 1 \rightarrow \sum_{j=1}^3 n_j$$



substitute

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{2\delta}} \left[\int_{\Gamma_\delta} \underline{t}(n, \underline{x}) dA + \sum_{j=1}^3 \int_{\Gamma_\delta} \underline{t}_n(-e_j, \underline{x}) n_j dA \right] = 0$$

$$\lim_{\delta \rightarrow 0} \frac{1}{A_{2\delta}} \int_{\Gamma_\delta} \underline{t}(n, \underline{x}) + \sum_{j=1}^3 \underline{t}(-e_j, \underline{x}) n_j dA = 0$$

as the tetrahedron is arbitrary the integrand must be zero

$$\underline{t}(n, \underline{x}) + \sum_{j=1}^3 \underline{t}(-e_j, \underline{x}) n_j = 0$$

use law of addition-reduction

$$\boxed{\underline{t}(n, \underline{x}) = \sum_{j=1}^3 \underline{t}(e_j, \underline{x}) n_j}$$

$$n = n_i; e_i$$

Use definition of dyadic product

$$\begin{aligned} (\underline{t}(e_j, \underline{x}) \otimes e_j) n &= (e_j \cdot n) \underline{t}(e_j, \underline{x}) \\ &= e_j \cdot (n_i e_i) \underline{t}(e_j, \underline{x}) \\ &= n_i \underbrace{e_j \cdot e_i}_{f_{ij}} \quad " \end{aligned}$$

$$= n_j \underline{t}(e_j, \underline{\alpha})$$

So we have

$$\begin{aligned}\underline{t}(n, \underline{\alpha}) &= (\underbrace{\underline{t}(e_j, \underline{\alpha})}_{\equiv n} \otimes e_j) n \\ &= \underline{\alpha} n\end{aligned}$$

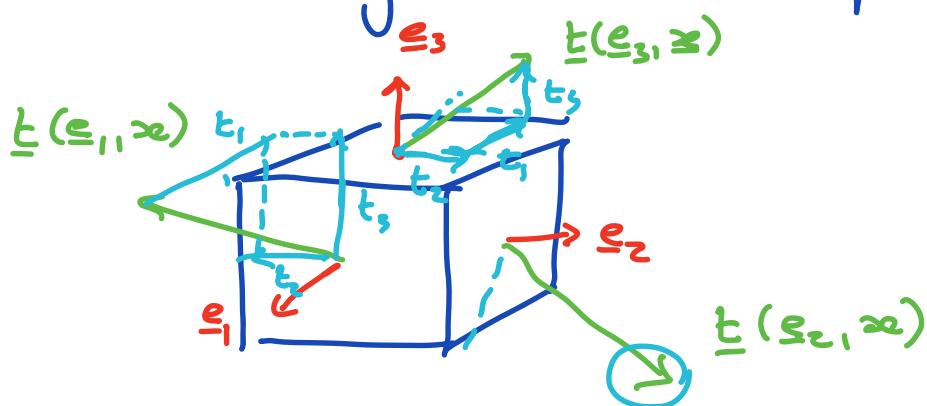
$$\Rightarrow \underline{\alpha} = \underline{t}(e_j, \underline{\alpha}) \otimes e_j$$

$$\text{traction} \cdot \underline{t}(e_j, \underline{\alpha}) = t_i(e_j, \underline{\alpha}) e_i \quad \underline{\alpha} = a_i e_i$$

$$\underline{\alpha} = t_i(e_j, \underline{\alpha}) e_i \otimes e_j$$

$$\alpha_{ij} = t_i(e_j, \underline{\alpha})$$

Hence α_{ij} is the i-th component of the traction on the j-th coordinate plane.



$$\underline{\underline{E}} = \begin{bmatrix} \underline{t}_1(\underline{e}_1, \underline{x}) & \underline{t}_1(\underline{e}_2, \underline{x}) & \underline{t}_1(\underline{e}_3, \underline{x}) \\ \underline{t}_2(\underline{e}_1, \underline{x}) & \underline{t}_2(\underline{e}_2, \underline{x}) & \underline{t}_2(\underline{e}_3, \underline{x}) \\ \underline{t}_3(\underline{e}_1, \underline{x}) & \underline{t}_3(\underline{e}_2, \underline{x}) & \underline{t}_3(\underline{e}_3, \underline{x}) \end{bmatrix}$$

$$\underline{t}_n = \underline{\underline{E}} \underline{n}$$