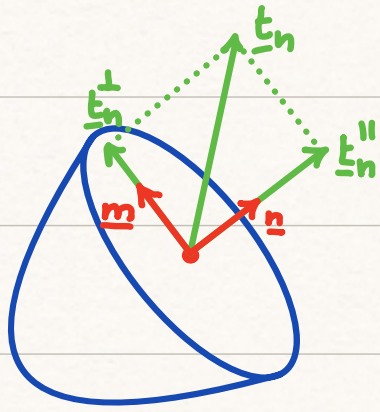


# Normal and Shear Stresses



Consider an arbitrary surface in  $B$  with normal  $\underline{n}$ . Then we have the two projection matrices

$$\underline{\underline{P}}'' = \underline{n} \otimes \underline{n} \quad \text{and} \quad \underline{\underline{P}}^\perp = \underline{\underline{I}} - \underline{n} \otimes \underline{n} = \underline{m} \otimes \underline{m}$$

that define the

$$\text{normal stress: } \underline{t}_n'' = \underline{\underline{P}}'' \underline{t}_n = (\underline{n} \cdot \underline{t}_n) \underline{n} = \sigma_n \underline{n}$$

$$\text{shear stress: } \underline{t}_n^\perp = \underline{\underline{P}}^\perp \underline{t}_n = (\underline{m} \cdot \underline{t}_n) \underline{m} = \tau \underline{m}$$

The magnitudes of these stresses are

$$\sigma_n = \underline{n} \cdot \underline{t}_n = \underline{n} \cdot \underline{\sigma} \underline{n} \quad \text{or} \quad \sigma_n = n_i \sigma_{ij} n_j$$

$$\tau = \underline{m} \cdot \underline{t}_n = \underline{m} \cdot \underline{\sigma} \underline{n} \quad \text{or} \quad \tau = m_i \sigma_{ij} n_j$$

If  $\sigma_n > 0$  the normal stresses are tensile if  $\sigma_n < 0$  the normal stresses are compressive.

$$\text{From geometry: } \underline{t}_n = \underline{t}_n'' + \underline{t}_n^\perp$$

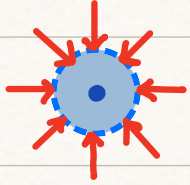
$$|\underline{t}_n|^2 = |\underline{\sigma}_n \underline{n}|^2 + |\tau \underline{n}|^2 = \sigma_n^2 + \tau^2$$

# Simple states of stress

## I) Hydrostatic stress

$$\underline{\underline{\sigma}} = -p \underline{\underline{I}} = \begin{bmatrix} -p & 0 & 0 \\ 0 & -p & 0 \\ 0 & 0 & -p \end{bmatrix}$$

$$\Rightarrow \underline{t}_n = \underline{\underline{\sigma}} \underline{n} = -p \underline{n} \quad \text{for all } \underline{n}$$



$$\underline{t}_n^{\parallel} = \underline{\underline{P}}_n^{\parallel} \underline{t} = (\underline{n} \otimes \underline{n}) (-p \underline{n}) = -p (\underline{n} \cdot \underline{n}) \underline{n} = -p \underline{n}$$

$$\Rightarrow \underline{t}_n = \underline{t}_n^{\parallel} \quad \underline{t}_n^{\perp} = 0$$

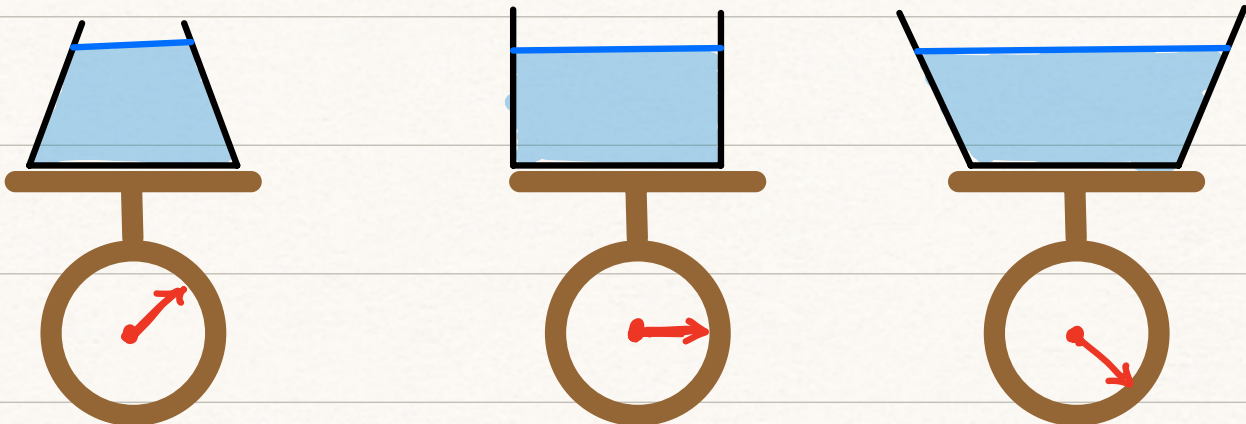
normal stress:  $\sigma_n = -p$   
shear stress:  $\tau = 0$  } on all planes

## Pascal's law:

The pressure in a fluid at rest is independent of the direction of a surface. Pressure is a scalar!

## Hydrostatic paradox: (Blaise Pascal)

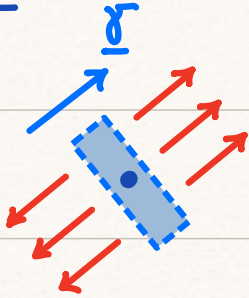
Weight different but the force on base is same  $f = pA$



## II) Uniaxial stress

$$\underline{\underline{\sigma}} = \sigma \underline{\underline{\gamma}} \otimes \underline{\underline{\gamma}}$$

( $\underline{\underline{\gamma}}$  is unit vector)



$$\Rightarrow \underline{\underline{t}}_n = \underline{\underline{\sigma}} \underline{\underline{n}} = \sigma (\underline{\underline{\gamma}} \cdot \underline{\underline{n}}) \underline{\underline{\gamma}}$$

Traction is always parallel to  $\underline{\underline{\gamma}}$

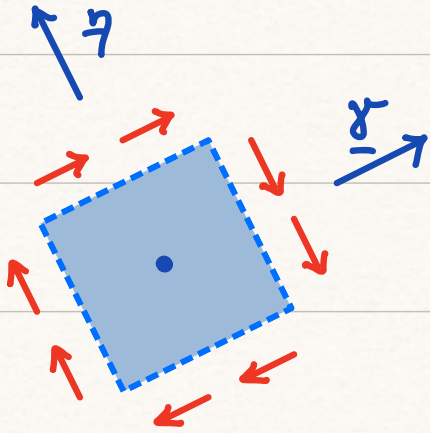
and vanished on surfaces with normal perpendicular to  $\underline{\underline{\gamma}}$ .

$\sigma > 0$  : pure tension

$\sigma < 0$  : pure compression

### III, Pure shear stress $\underline{\gamma} \cdot \underline{\eta} = 0$

$$\underline{\underline{\sigma}} = \tau (\underline{\gamma} \otimes \underline{\eta} + \underline{\eta} \otimes \underline{\gamma}) \Rightarrow \underline{t}_n = \underline{\underline{\sigma}} \underline{n} = \tau (\underline{\eta} \cdot \underline{n}) \underline{\gamma} + \tau (\underline{\gamma} \cdot \underline{n}) \underline{\eta}$$



$$\underline{n} = \underline{\eta}: \underline{t}_n = \tau \underline{\gamma}$$

$$\underline{n} = \underline{\gamma}: \underline{t}_n = \tau \underline{\eta}$$

### IV, Plane stress

If there exists a pair of orthogonal vectors  $\underline{\gamma}$  and  $\underline{\eta}$  such that the matrix representation of  $\underline{\underline{\sigma}}$  in the frame  $\{\underline{\gamma}, \underline{\eta}, \underline{\gamma} \times \underline{\eta}\}$  is of the form

$$[\underline{\underline{\sigma}}] = \begin{pmatrix} \sigma_{11} & \sigma_{12} & 0 \\ \sigma_{21} & \sigma_{22} & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

then a state of plane stress exists.

Q: Is uniaxial stress a plane stress?

$$\underline{\underline{\underline{\sigma}}} = \sigma \underline{\underline{a}} \otimes \underline{\underline{a}}$$

Pick a frame  $\{\underline{e}_i\}$  and evaluate  $[\underline{\underline{\sigma}}]$ .

What frame  $\underline{e}_1 = \underline{a}$  know  $\underline{e}_2 \cdot \underline{a} = \underline{e}_3 \cdot \underline{a} = 0$

$$\sigma_{ij} = \underline{e}_i \cdot \underline{\underline{\underline{\sigma}}} \underline{e}_j$$

substitute with  $\underline{a} = \underline{e}_1$

$$\begin{aligned} \sigma_{ij} &= \underline{e}_i \cdot (\sigma \underline{\underline{e}}_1 \otimes \underline{\underline{e}}_1) \underline{e}_j \\ &= \sigma \underline{e}_i \cdot (\underline{e}_1 \cdot \underline{e}_j) \underline{e}_1 = \sigma (\underline{e}_i \cdot \underline{e}_1) (\underline{e}_j \cdot \underline{e}_1) \end{aligned}$$

$$\sigma_{11} = \sigma (\underline{e}_1 \cdot \underline{e}_1) (\underline{e}_1 \cdot \underline{e}_1) = \sigma$$

$$\sigma_{12} = \sigma (\underline{e}_1 \cdot \underline{e}_1) (\underline{e}_1 \cdot \underline{e}_2) = 0$$

$$\sigma_{22} = \sigma (\underline{e}_2 \cdot \underline{e}_1) (\underline{e}_1 \cdot \underline{e}_2) = 0$$

...

$$\Rightarrow [\underline{\underline{\underline{\sigma}}}] = \begin{bmatrix} \sigma & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad \checkmark \text{ plane stress}$$

# Extremal Stress Values

## I, Maximum and Minimum Normal Stresses

Given a state of stress  $\underline{\underline{\sigma}}$  at point  $\underline{x}$ , what are the unit normals  $\underline{n}$  corresponding to min. and max. normal stress  $\sigma_n$ .

This is a constrained optimization problem, because we want to find extrema of the function  $\sigma_n = \sigma_n(\underline{n})$  with the constraint that  $|\underline{n}| = 1$ .

Lagrange multiplier method

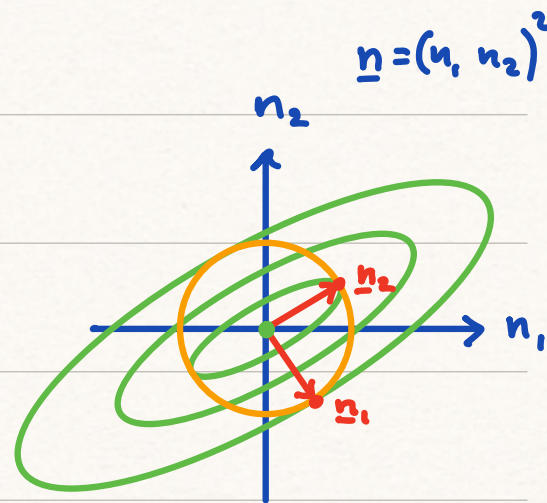
$$\mathcal{L}(\underline{n}, \lambda) = \underline{n} \cdot \underline{\underline{\sigma}} \underline{n} - \lambda (\underline{n} \cdot \underline{n} - 1)$$

$$\mathcal{L}(n_i, \lambda) = n_i \sigma_{ij} n_j - \lambda (n_i n_i - 1)$$

function

constraint

Lagrange multiplier



$f(\underline{n}) = \underline{n} \cdot \underline{\underline{\sigma}} \underline{n}$  is quadratic

Function  $f(\underline{n}) = \underline{n} \cdot \underline{\underline{\sigma}} \underline{n}$  is quadratic in components of  $\underline{n}$ .

If eigenvalues of  $\underline{\underline{\sigma}}$  are positive then the level sets of  $f(\underline{n})$  are ellipsoids as shown.

The extremal values are the stationary points of  $\mathcal{L}(\underline{n}, \lambda)$

$$\frac{\partial \mathcal{L}}{\partial \lambda} = n_i n_i - 1 = 0$$

$$\frac{\partial \mathcal{L}}{\partial n_k} = \sigma_{ij} (n_{i,k} n_j + n_i n_{j,k}) - \lambda (2 n_i n_{i,k}) = 0$$

$$\text{where } n_{i,k} = \delta_{ik} \quad n_{j,k} = \delta_{jk}$$

$$= \sigma_{ij} (\delta_{ik} n_j + \delta_{jk} n_i) - \lambda (2 n_i \delta_{ik})$$

$$= \sigma_{kj} n_j + \sigma_{ik} n_i - 2 \lambda n_k \stackrel{\sigma_{ik} = \sigma_{ki}}{\downarrow} = \sigma_{kj} n_j + \sigma_{ki} n_i - 2 \lambda n_k$$

$$= 2 (\sigma_{ik} n_k - \lambda n_k) = 0$$

In symbolic notation:  $(\underline{\underline{\sigma}} - \lambda \underline{\underline{I}}) \underline{\underline{n}} = \underline{\underline{0}}$  and  $|\underline{\underline{n}}| = 1$

The Lagrange multiplier method leads to an eigen problem, where the Lagrange multiplier,  $\lambda$ , is the eigenvalue and the normal,  $\underline{n}$ , the eigenvector.

We can see that  $\lambda$  is the magnitude of the normal stress by taking the dot product of eigenproblem with  $\underline{n}$ .

$$\underline{\underline{n}} \cdot (\underline{\underline{\sigma}} - \lambda \underline{\underline{I}}) \underline{\underline{n}} = 0 \Rightarrow \underline{\underline{n}} \cdot \underline{\underline{\sigma}} \underline{\underline{n}} = \lambda \underline{\underline{n}} \cdot \underline{\underline{n}} \Rightarrow \sigma_n = \lambda$$

Hence to find the extremal stress values we must find the eigenvalues  $\lambda_i$  and eigenvectors  $\underline{n}_i$ .

$\lambda_i$ 's are the principal normal stresses  $\Rightarrow \lambda_i = \sigma_i$

$\underline{n}$ 's are the principal directions of  $\underline{\underline{\sigma}}$

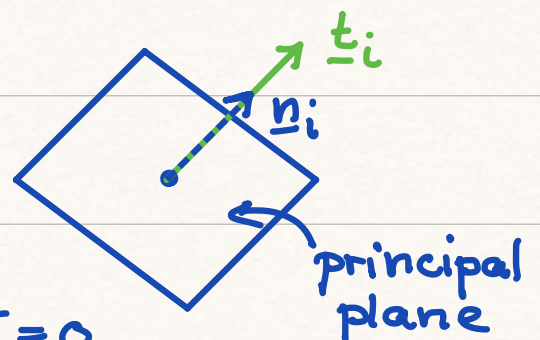
Since  $\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T$  all  $\lambda_i$  are real and the set  $\{\underline{n}_i\}$  form a mutually orthogonal basis, so that  $\underline{\underline{\sigma}}$  can be represented as  $\underline{\underline{\sigma}} = \sum_{i=1}^3 \sigma_i \underline{n}_i \otimes \underline{n}_i$

The tractions in the principal directions are

$$\underline{t}_{\underline{n}_i} = \underline{\underline{\sigma}} \underline{n}_i = \sigma_i \underline{n}_i$$

Since  $\underline{t}_i \parallel \underline{n}_i$  there is no shear

stress on the principal planes,  $\underline{t}_i^\perp = 0$ .



If the  $\sigma_i$ 's are distinct and ordered  $\sigma_1 > \sigma_2 > \sigma_3$

then  $\sigma_1$  and  $\sigma_3$  are the max. and min. normal stresses.



## II. Maximum and minimum shear stresses

Given the principal directions  $\underline{n}_1, \underline{n}_2$  and  $\underline{n}_3$  at  $\underline{x}$  what is the unit vector  $\underline{s} = [s_1, s_2, s_3]$  that gives the max. and min. values of the shear stresses  $\tau$ ?

In the frame of the principal directions  $\{\underline{n}_i\}$

$$\underline{s} = s_i \underline{n}_i \quad \text{where} \quad s_i = \underline{s} \cdot \underline{n}_i$$

so that the traction vector in direction  $\underline{s}$  is

$$\begin{aligned} \underline{t}_s &= \underline{\sigma} \underline{s} = \sum_{i=1}^3 \sigma_i \underline{n}_i \otimes \underline{n}_i s_j \underline{n}_j \\ &= \sum_{i=1}^3 \sigma_i s_j (\underline{n}_i \otimes \underline{n}_j) \underline{n}_j = \sum_{i=1}^3 \sigma_i s_j \underbrace{(\underline{n}_i \cdot \underline{n}_j)}_{\delta_{ij}} \underline{n}_i \\ &= \sum_{i=1}^3 \sigma_i s_i \underline{n}_i \end{aligned}$$

traction vector associated with  $\underline{s}$  is

$$\underline{t}_s = \sigma_1 s_1 \underline{n}_1 + \sigma_2 s_2 \underline{n}_2 + \sigma_3 s_3 \underline{n}_3$$

The magnitudes of normal,  $\sigma_n$ , and shear stress,  $\tau$ , are

$$\sigma_n = \underline{s} \cdot \underline{t}_s = \sigma_1 s_1^2 + \sigma_2 s_2^2 + \sigma_3 s_3^2$$

$$\tau^2 = |\underline{t}_s|^2 - \sigma_n^2 = \sigma_1^2 s_1^2 + \sigma_2^2 s_2^2 + \sigma_3^2 s_3^2 - (\sigma_1 s_1^2 + \sigma_2 s_2^2 + \sigma_3 s_3^2)^2$$

Hence we have the following expression for the shear stress

$$\tau^2 = \sum_{i=1}^3 \sigma_i^2 s_i^2 - \left( \sum_{i=1}^3 \sigma_i s_i^2 \right)^2$$

we are looking for the extremal values of  $\tau^2$

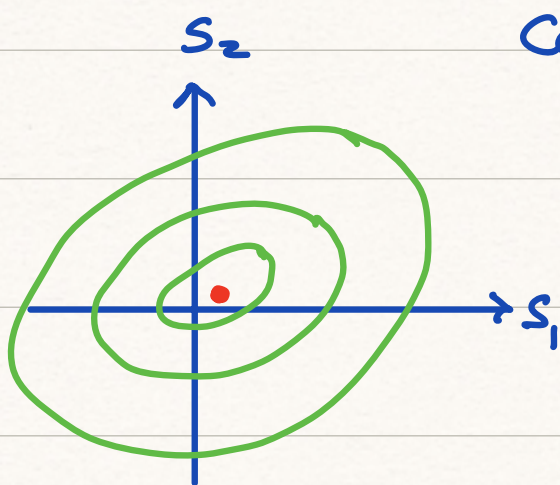
under the constraint  $|\underline{s}|^2 = 1 \rightarrow s_1^2 + s_2^2 + s_3^2 = 1$

$\Rightarrow$  Solve using Lagrange mult. or direct elimination.

I) Eliminate  $s_3^2 = 1 - s_1^2 - s_2^2 \Rightarrow \tau^2 = \tau^2(s_1, s_2)$ .

$$\tau^2 = \sigma_1^2 s_1^2 + \sigma_2^2 s_2^2 + \sigma_3^2 s_3^2 - (\sigma_1 s_1^2 + \sigma_2 s_2^2 + \sigma_3 s_3^2)^2$$

$$= \sigma_1^2 s_1^2 + \sigma_2^2 s_2^2 + \sigma_3^2 (1 - s_1^2 - s_2^2) - (\sigma_1 s_1^2 + \sigma_2 s_2^2 + \sigma_3 (1 - s_1^2 - s_2^2))^2$$



Constraint  $|\underline{s}| = 1$  is incorporated

To find extremum

partial derivatives need

to vanish.

We just need to find  $\frac{\partial \tau^2}{\partial s_1} = \frac{\partial \tau^2}{\partial s_2} = 0$ .

$$\frac{\partial \tau^2}{\partial s_1} = 2s_1(\sigma_1 - \sigma_3) \left\{ \sigma_1 - \sigma_3 - 2[(\sigma_1 - \sigma_3)s_1^2 + (\sigma_2 - \sigma_3)s_2^2] \right\} = 0$$

$$\frac{\partial \tau^2}{\partial s_2} = 2s_2(\sigma_2 - \sigma_3) \left\{ \sigma_2 - \sigma_3 - 2[(\sigma_1 - \sigma_3)s_1^2 + (\sigma_2 - \sigma_3)s_2^2] \right\} = 0$$

First solution:  $s_1 = s_2 = 0 \Rightarrow s_3 = 1 \quad \underline{s} = \pm \underline{n}_3$

$$\tau^2 = \sigma_3^2 \cdot 1 - (\sigma_3 \cdot 1)^2 = 0$$

$\Rightarrow$  minimum in the shear stress

which vanishes on principal plane

Second solution:  $s_1 = 0$

$$\frac{\partial \tau^2}{\partial n_2} = \sigma_2 - \sigma_3 - 2[(\sigma_2 - \sigma_3)s_2^2] = 0$$

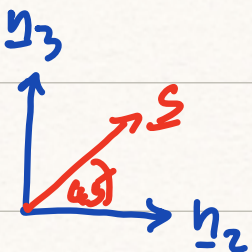
$$(\sigma_2 - \sigma_3)(1 - 2s_2^2) = 0 \Rightarrow s_2 = \pm \frac{1}{\sqrt{2}}$$

from  $s_2^2 + s_3^2 = 1 \Rightarrow s_3 = \pm \frac{1}{\sqrt{2}}$

$$\Rightarrow \underline{s} = \pm \frac{1}{\sqrt{2}} \underline{n}_2 \pm \frac{1}{\sqrt{2}} \underline{n}_3$$

$$\tau^2 = \frac{\sigma_2^2}{2} + \frac{\sigma_3^2}{2} - \left( \frac{\sigma_2}{2} + \frac{\sigma_3}{2} \right)^2$$

$$= \frac{\sigma_2^2}{2} + \frac{\sigma_3^2}{2} - \left( \frac{\sigma_2^2}{4} + 2 \frac{\sigma_2}{2} \frac{\sigma_3}{2} + \frac{\sigma_3^2}{4} \right)$$



$$\tau^2 = \left(\frac{\sigma_2}{2}\right)^2 - 2 \frac{\sigma_2}{2} \frac{\sigma_3}{2} + \left(\frac{\sigma_3}{2}\right)^2 = \left(\frac{\sigma_2 - \sigma_3}{2}\right)^2$$

We have the following two solutions:

$$\text{min. } \tau = 0 \quad \text{for } \underline{s} = \pm \underline{n}_3$$

$$\text{max. } \tau = \frac{1}{2}(\sigma_2 - \sigma_3) \quad \text{for } \underline{s} = \pm \frac{\underline{n}_2}{\sqrt{2}} \pm \frac{\underline{n}_3}{\sqrt{2}}$$

Two additional pairs of solutions can be obtained by eliminating  $\underline{n}_1$  or  $\underline{n}_2$  from  $\tau^2$  and following similar steps. So that we have

Minimum shear stresses:

$$\tau = 0 \quad \text{on } \underline{s} = \pm \underline{n}_1 \quad \underline{s} = \pm \underline{n}_2 \quad \underline{s} = \pm \underline{n}_3$$

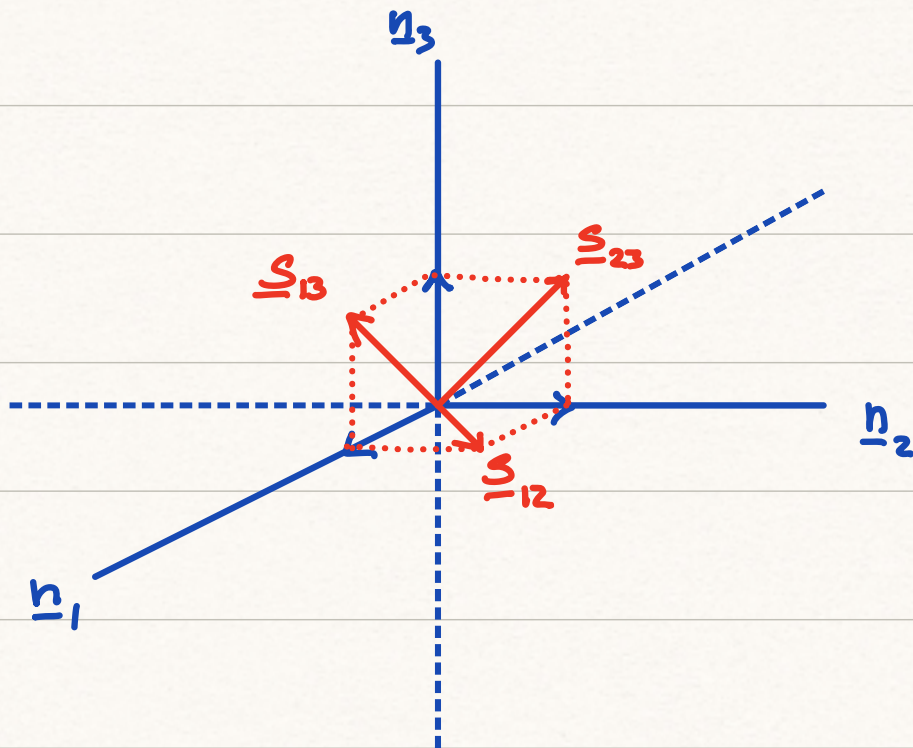
Maximum shear stresses:

$$\tau_{23} = \frac{1}{2}(\sigma_2 - \sigma_3) \quad \text{on } \underline{s}_{23} = \frac{1}{\sqrt{2}}(\pm \underline{n}_2 \pm \underline{n}_3)$$

$$\tau_{13} = \frac{1}{2}(\sigma_1 - \sigma_3) \quad \text{on } \underline{s}_{13} = \frac{1}{\sqrt{2}}(\pm \underline{n}_1 \pm \underline{n}_3)$$

$$\tau_{12} = \frac{1}{2}(\sigma_1 - \sigma_2) \quad \text{on } \underline{s}_{12} = \frac{1}{\sqrt{2}}(\pm \underline{n}_1 \pm \underline{n}_2)$$

where we assume  $\sigma_1 \geq \sigma_2 \geq \sigma_3$



Note: G&S do this with Lagrange multipliers but it leads to odd expressions in index notation, such as

$$4 \left( \sum_{j=1}^3 n_j^2 \sigma_j \right) n_i \sigma_i = 2\lambda n_i \quad ?$$

where 'i' seems to be a dummy on the l.h.s. but a free index on the r.h.s.

⇒ we did it the pedestrian way.