

Lecture 16: Unconfined flow continued

Logistics: - Please complete HW5

- HW6 is up (Problems?)

etg_num

shift by $\frac{\Delta x}{2}$

QC: add form of $\Pi =$

Last time: Numerical solution for steady unconfined flow

$$\text{Continuous PDE: } -\nabla \cdot [h \nabla h] = 1$$

$$\text{Discrete residual: } \underline{r} = \underline{D} [\{ \underline{M} \underline{h} \}_f \underline{G} \underline{h}] - \underline{f}$$

$$\text{Directional derivative: } \underline{D}_{\hat{h}} \underline{r}(\underline{h}) = \left. \frac{d}{d\epsilon} \underline{r}(\underline{h} + \epsilon \hat{h}) \right|_{\epsilon=0} = \underline{J}(\underline{h}) \hat{h}$$

Jacobian for unconfined flow:

$$\underline{J} = \underline{D} [\{ \underline{M} \underline{h} \}_f \underline{G} + \{ \underline{G} \underline{h} \}_f \underline{M}]$$

Newton-Raphson method:

$$dh^k = - \underline{J}(\underline{h}^k)^{-1} \underline{r}(\underline{h}^k)$$

$$\underline{h}^{k+1} = \underline{h}^k + dh^k$$

1 Discretize then linearize

2 Linearize then discretize

→ Functional derivative

get the same result

Today: Continue discussion of unconfined flow

- Flux computation
- unconfined flow on spherical shell
- Numerical approximation of Jacobian
- Transient unconfined flow
- Example: Drainage of unconfined aquifer

Flux computation

$$-\nabla \cdot (h' \nabla h') = 1$$

$$\nabla \cdot (\underbrace{h' \underline{q}'}_{\underline{Q}}) = 1$$

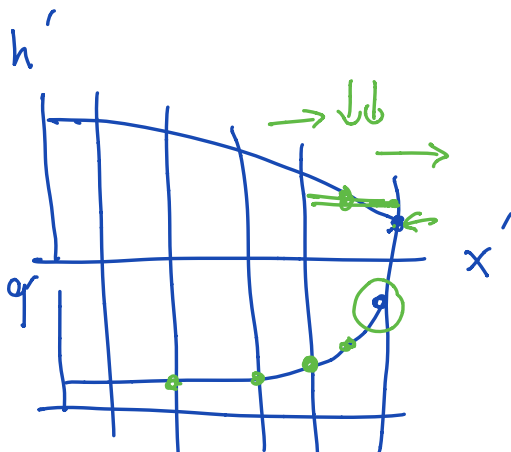
$$\nabla \cdot \underline{Q} = 1$$

$$\frac{d\underline{Q}}{dx} = 1$$

⇒ update comp flux

to compute $\underline{Q}' = h' \underline{q}'$

$$\underline{q}' = -\nabla h'$$



⇒ conservative out/inflow on band

(but to get q exact we need additional h unknown on band)

Unconfined flow on spherical shell

⇒ because geometry is hidden in \underline{D} , \underline{G}

the Jacobian \underline{J} stays the same!

⇒ Newton-Raphson is no problem

Solu for steady unconfined flow with precip.

$$\text{PDE: } -\frac{1}{R \sin \theta} \frac{d}{d\theta} \left[\sin \theta \frac{k}{R} h \frac{dh}{d\theta} \right] = q_p \quad \theta \in [\theta_1, \theta_2]$$

$$\text{BC's: } \left. \frac{dh}{d\theta} \right|_{\theta_1} = 0 \quad h(\theta_2) = h_b$$

dimensionless head: $h' = \frac{h}{h_c}$

$$-\frac{d}{d\theta} \left[\sin \theta h' \frac{dh'}{d\theta} \right] = \frac{q_p R^2}{k h_c^2} = 1 \Rightarrow$$

$$h_c = \sqrt{\frac{q_p R^2}{k}}$$

$$h \frac{dh}{d\theta} = \frac{1}{2} \frac{dh^2}{d\theta} = \frac{1}{2} \frac{du}{d\theta} \\ u = h^2$$

Dimensionless problem:

$$\text{PDE} \quad -\frac{d}{d\theta} \left[\sin\theta h' \frac{dh'}{d\theta} \right] = \sin\theta \quad \theta \in [0, \theta_b]$$

$$\text{BC:} \quad \left. \frac{dh'}{d\theta} \right|_0 = 0 \quad h'(\theta_b) = \Pi = \frac{h_b}{h_c}$$

$$\text{Integrate:} \quad -\sin\theta h' \frac{dh'}{d\theta} = -\cos\theta - c_1$$

$$\text{New BC:} \quad 0 = -\cancel{\cos 0} - c_1 \Rightarrow c_1 = -1$$

$$-\sin\theta h' \frac{dh'}{d\theta} = -\cos\theta + 1$$

$$\sin\theta h' \frac{dh'}{d\theta} = \cos\theta - 1$$

$$q' = -\frac{dh'}{d\theta}$$

Integrate:

$$h' dh' = \left(\frac{\cos\theta}{\sin\theta} - \frac{1}{\sin\theta} \right) d\theta = (\cot\theta - \csc\theta) d\theta$$

$$\frac{h'^2}{2} = \log(\cos\theta + 1) + c_2$$

$$\text{Dir BC:} \quad \frac{\Pi^2}{2} = \log(\cos\theta_b + 1) + c_2$$

$$c_2 = \frac{\Pi^2}{2} - \log(\cos\theta_b + 1)$$

$$h' = \sqrt{\Pi^2 + 2 \log\left(\frac{\cos\theta + 1}{\cos\theta_b + 1}\right)}$$
$$q' = -\frac{dh'}{d\theta} = \frac{1 - \cos\theta}{h'(\theta) \sin\theta}$$

$$Q' = h' q' = \frac{1 - \cos \theta}{\sin \theta}$$

Spherical shell Newton see line script

Num. Newton see line script.

Transient unconfined flow

(following Zhang et al 2013)

Let's consider an aquifer
with vertical variation

in $k(z) = k_0 z^n$ and $\phi(z) = \phi_0 z^m$

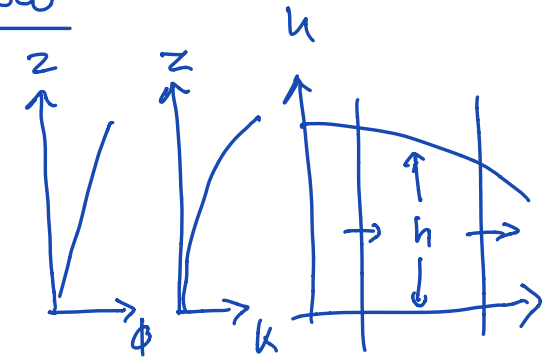
typically $n/m \in [2, 3]$

$\Rightarrow k \sim \phi^2$ or ϕ^3

The balance of fluid mass is

$$\frac{\partial}{\partial t} \int_0^h \phi dz + \nabla \cdot \int_0^h q(z) dz = f_s$$

where h is water table $q = -K(z) \nabla h$



Accumulation term

$$\int_0^h \phi(z) dz = \phi_0 \int_0^h z^m dz = \frac{\phi_0}{m+1} z^{m+1} \Big|_0^h = \frac{\phi_0}{m+1} h^{m+1}$$

$$\frac{\partial}{\partial t} \int_0^h \phi(z) dz = \frac{\phi_0}{m+1} \frac{\partial h^{m+1}}{\partial t} = \phi_0 h^m \frac{\partial h}{\partial t} = \phi(h) \frac{\partial h}{\partial t}$$

$\Rightarrow \phi(h) \rightarrow$ is unconfined storage

Flux term:

$$\nabla \cdot \int_0^h q(z) dz = -\frac{k_0}{n+1} h^{n+1} \nabla h$$

Governing equation

$$\frac{\partial h^{m+1}}{\partial t} - D_h \nabla \cdot [h^{n+1} \nabla h] = f_s$$

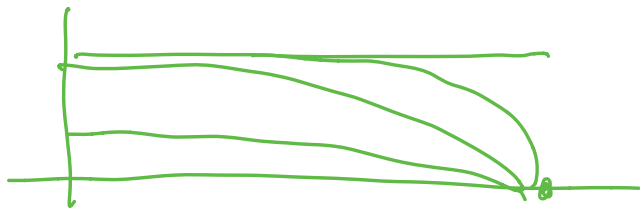
unconfined hydr. diff. : $D_h = \frac{k_0 (m+1)}{\phi_0 (n+1)}$

limiting case: $m=0$ $n=0 \Rightarrow \phi = \phi_0$ $k = k_0$

$$\frac{\partial h}{\partial t} - \underbrace{D_h \nabla \cdot [h \nabla h]}_{\text{steady term we have worked with}} = f_s$$

steady term we have worked with

Next time



self-similar solution