

## Temperature-dependent viscosity

Common source of non-linearity is the variation of viscosity with temperature.

Ice rheology is complex and depends on the microscopic deformation mechanism.

We consider "diffusion creep" which results in a Newtonian rheology.

$$\mu = \frac{RTd^2}{42V_m D_{0,v}} \exp\left(\frac{E_A}{RT}\right)$$

Parameters:  $d$  = grain diameter  $\sim 1 \text{ mm}$

$T$  = temperature

$V_m$  = molar volume  $1.97 \cdot 10^{-5} \frac{\text{m}^3}{\text{mol}}$

$D_{0,v}$  = vol. diff. constant  $9.1 \cdot 10^{-4} \frac{\text{m}^2}{\text{s}}$

$E_A$  = vol. diff. act. energy  $59.4 \frac{\text{kJ}}{\text{mol}}$

$R$  = mol. gas constant  $8.314 \frac{\text{J}}{\text{K mol}}$

Newtonian because  $\mu \neq \mu(\dot{\gamma})$  !

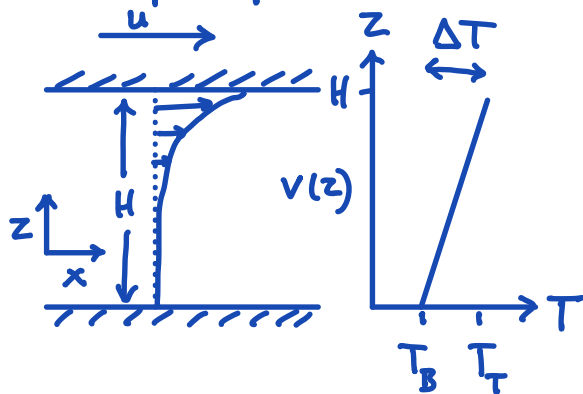
But  $\mu$  has Arrhenius dependence on  $T$

The temperature-dependence of the pre-exponential factor is often neglected.

$$\mu = \mu_0 \exp\left(\frac{E_A}{RT}\right)$$

$$\mu_0 = \frac{RT_m d^2}{42 \nu_m D_{0,v}}$$

Example problem: Couette flow with  $T$  gradient



Boundary layer forms at the hot lower boundary where shear is localized.

In the absence of heating by viscous dissipation the  $T$ -field is independent of velocity

$\Rightarrow$  one-way coupling:  $v = v(T)$  but  $T \neq T(v)$

Viscous energy dissipation leads to two-way coupl.

Temperature field:  $\Delta T = T_T - T_B$

$$\nabla \cdot [\kappa \nabla T] = 0 \rightarrow \frac{d^2 T}{dz^2} = 0 \Rightarrow T = T_B + \frac{\Delta T}{H} z$$

Velocity & pressure fields:

$$-\nabla \cdot [\mu (\nabla \underline{v} + \nabla^T \underline{v})] + \nabla \pi = 0 \quad \pi = p + \rho g z$$

$$\nabla \cdot \underline{v} = 0$$

deviatoric stress in component form:

$$\underline{\underline{\tau}} = \mu (\nabla \underline{v} + \nabla^T \underline{v}) = \mu \begin{bmatrix} 2v_{x,x} & v_{x,z} + v_{z,x} \\ v_{x,z} + v_{z,x} & 2v_{z,z} \end{bmatrix}$$

From flow geometry:  $v_z = 0 \rightarrow v_{z,z} = v_{z,x} = 0$

$$v_{x,x} = 0 \quad (\text{from continuity})$$

$$\nabla \pi = \begin{pmatrix} \pi_{,x} \\ \pi_{,z} \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

$\Rightarrow$  all terms in z-momentum balance vanish

$$\boxed{-\frac{\partial}{\partial z} \left[ \mu \frac{\partial v}{\partial z} \right] + \frac{\partial \pi}{\partial x} = 0} \quad v = v_x$$

In Couette example the domain is infinite

in x-dir, so that  $\frac{\partial \pi}{\partial x} = 0$ .

Solve following ODE:

$$\frac{\partial}{\partial z} \left[ \mu(T(z)) \frac{\partial v}{\partial z} \right] = 0$$

$$v(0) = 0 \quad v(H) = u$$

where

$$\mu = \mu_0 \exp\left(\frac{E_a}{RT}\right)$$

$$T = T_B + \frac{\Delta T}{H} z$$

$$\Delta T = T_T - T_B > 0$$

Integrate once:

$$\mu \frac{\partial v}{\partial z} = c_1 \quad \text{here } c_1 = \tau = \text{shear stress}$$

$$\tau = \mu \frac{\partial v}{\partial z} \quad \text{is definition of } \mu!$$

Integrate once more:

$$v(z) = \tau \int_0^z \frac{dz}{\mu(T(z))}$$

$$v(z) = \tau \int_0^z \frac{dz}{\mu_0 \exp\left(\frac{E_a}{RT(z)}\right)} = \frac{\tau}{\mu_0} \int_0^z \exp\left(\frac{-E_a/R}{T(z)}\right) dz$$

$$v(z) = \frac{\tau}{\mu_0} \int_0^z \exp\left(\frac{-E_a/R}{T_B + \Delta T z/H}\right) dz$$

difficult integral, but if  $\Delta T \ll T_B$  the

exponential factor can be approximated as

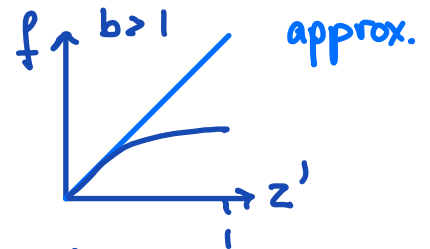
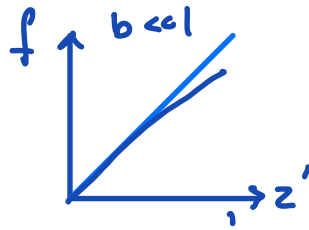
$$f(z) = -\frac{E_a}{RT_B} \frac{1}{1 + \frac{\Delta T}{T_B} \frac{z}{H}} = \frac{-a}{1 + bz'} \quad z' = \frac{z}{H} \quad a = \frac{E_a}{RT_B} \quad b = \frac{\Delta T}{T_B}$$

Taylor series expansion at  $z'=0$

$$\mathcal{L}_0 f(z) = f(0) + \left. \frac{df}{dz'} \right|_0 z' = -a + abz' = -a(1 - bz')$$

where  $\frac{df}{dz} = \frac{ab}{(1+bz')^2}$

so that we have



$$f(z) = -\frac{E_a}{RT_B} \frac{1}{1 + \frac{\Delta T}{T_B} \frac{z}{H}} \approx -\frac{E_a}{RT_B} \left( 1 - \frac{\Delta T}{T_B} \frac{z}{H} \right)$$

$$V(z) = \frac{\tau}{\mu_0} e^{-a} \int_0^z e^{abz'} dz \quad dz' = \frac{dz}{H} \quad dz = H dz'$$

$$V(z) = \frac{\tau H}{\mu_0} e^{-a} \int_0^{z'} e^{abz''} dz'' = \frac{\tau H}{\mu_0} \frac{e^{-a}}{ab} (e^{abz'} - e^0)$$

$$V(z') = \frac{\tau H}{\mu_0} \frac{e^{-a}}{ab} (e^{abz'} - 1)$$

1) Set velocity of top plate and find shear stress  $\tau$

2) Set shear stress  $\tau$  and find velocity of top plate

$$v(z'=1) = u = \frac{\tau H}{\mu_0} \frac{e^{-a}}{ab} (e^{ab} - 1)$$

$$\Rightarrow \tau = \frac{u \mu_0}{H} \frac{ab}{e^{-a}} \frac{1}{e^{ab} - 1}$$

substitute

$$\frac{v(z')}{u} = \frac{e^{abz'} - 1}{e^{ab} - 1} \quad \text{where } a = \frac{E_a}{RT_B} \quad b = \frac{\Delta T}{T_B} \quad z' = \frac{z}{H}$$

so that  $a \cdot b = \frac{E_a \Delta T}{RT_B^2}$

Hence the velocity profile is:

$$\boxed{\frac{v(z')}{u} = \frac{\exp\left(\frac{E_a \Delta T}{RT_B^2} \frac{z}{H}\right) - 1}{\exp\left(\frac{E_a \Delta T}{RT_B^2}\right) - 1}}$$

$$T = T_B + \frac{\Delta T}{H} z = T_B \left(1 + \frac{\Delta T}{T_B} \frac{z}{H}\right) = T_B \left(1 - \frac{T}{T_B} + 1\right)$$

$$\frac{T}{T_B} = 1 - bz'$$

corresponding viscosity

$$\mu = \mu_0 \exp\left(\frac{E_a}{RT}\right)$$

$$\frac{\mu}{\mu_0} = \exp\left(\frac{E_a}{RT_B} \frac{T_B}{T}\right) = \exp\left(\frac{E_a}{RT_B} \frac{1}{1 - bz'}\right) = \exp\left(\frac{a}{1 - bz'}\right)$$