

Lecture 27: Darcy-Stokes II

Logistics: - sorry still didn't have time
to fix HW

- CIS please fill out

Last time: - Deriving Darcy-Stokes equation

- Briefly reviewed simplified model

- Two phase mass conservation

$$\nabla \cdot [\phi \underline{v}_f + (1-\phi) \underline{v}_s] = \nabla \cdot [\underline{q}_r + \underline{v}_s] = - \frac{\Delta p}{\rho \phi \beta_s} \tau$$

- Two phase lin. mom. balance

$$\nabla \cdot [\phi \underline{\underline{\sigma}}_f + (1-\phi) \underline{\underline{\sigma}}_s] = \bar{\rho} g \hat{z}$$

- Newtonian viscous stress

$$\underline{\underline{\sigma}} = -p \underline{\underline{I}} + \underline{\underline{\tau}}$$

$$p = -\frac{1}{3} \text{tr}(\underline{\underline{\sigma}}) \quad \nabla \cdot \underline{v} = 0$$

$$\underline{\underline{\tau}} = \mu \left(\underline{\underline{\nabla}} \underline{v} + \underline{\underline{\nabla}}^T \underline{v} - \frac{2}{3} \underline{\underline{\nabla}} \cdot \underline{v} \underline{\underline{I}} \right) = 2\mu \underline{\underline{\dot{\sigma}}}$$

Today: - Compressible fluid

- Darcy Stokes system

Compressible Newtonian Fluid

General compressible Cauchy stress tensor

$$\underline{\underline{\sigma}} = -p \underline{\underline{I}} + 2\mu \underline{\underline{\dot{\epsilon}}} + \lambda \nabla \cdot \underline{\underline{v}} \underline{\underline{I}}$$

p = thermodynamic pressure (eqbm) $p = p(p)$

μ = shear viscosity

λ = second viscosity (related to compression)

Mechanical pressure / mean stress:
isotropic

$$p_m = -\frac{1}{3} \text{tr}(\underline{\underline{\sigma}}) = -\frac{1}{3} \text{tr}[-p \underline{\underline{I}} + \lambda \nabla \cdot \underline{\underline{v}} \underline{\underline{I}} + 2\mu \underline{\underline{\dot{\epsilon}}}]$$

$$= p - \lambda \nabla \cdot \underline{\underline{v}} - \frac{2}{3} \mu \nabla \cdot \underline{\underline{v}}$$

$$= p - \underbrace{\left(\lambda + \frac{2}{3} \mu\right)}_{\text{bulk viscosity } \xi} \nabla \cdot \underline{\underline{v}}$$

$$\text{bulk viscosity } \xi = \lambda + \frac{2}{3} \mu$$

$$p_m = p - \xi \nabla \cdot \underline{\underline{v}}$$

dynamic pressure

In compressible flow the mean stress / mech. pressure differs from thermodynamic, eqbm pressure

in divergent flows $p_m < p$

Two pressures are equal if:

$$\nabla \cdot \underline{v} = 0 \quad \text{or} \quad \xi = 0$$

Rewrite the Cauchy stress as:

$$\underline{\underline{\sigma}} = - \underbrace{(\rho - \xi \nabla \cdot \underline{v})}_{p_w} \underline{\underline{I}} + \mu (\nabla \underline{v} + \nabla^T \underline{v})$$

lin. mom. balance:

$$-\nabla \cdot \underline{\underline{\sigma}} + \rho g \hat{z} = 0 \quad \nabla \cdot [f \underline{\underline{I}}] = \nabla f$$

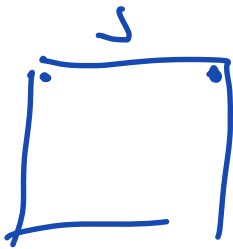
$$-\nabla \cdot [\mu (\nabla \underline{v} + \nabla^T \underline{v})] + \nabla \cdot [(\rho - \xi \nabla \cdot \underline{v}) \underline{\underline{I}}] + \rho g \hat{z} = 0$$

Mass balance: $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{v}) = 0$

what is relation between ρ and ξ

$$\rho = \rho_0 + \xi (\rho - \rho_0)$$

$\rho =$ therm. pressure



$$-\nabla \cdot [\mu (\nabla \underline{v} + \nabla^T \underline{v})] + \nabla \cdot (\underline{\rho - \xi \nabla \cdot \underline{v}}) + \rho g \hat{z} = 0$$

$$\xi = 0: -\nabla \cdot [\mu (\nabla \underline{v} + \nabla^T \underline{v})] + \nabla p + \rho g \hat{z} = 0$$

Two-phase Darcy-Stokes

Total momentum balance:

$$\nabla \cdot [\phi \underline{\underline{\sigma}}_f + (1-\phi) \underline{\underline{\sigma}}_s] = \rho g \hat{z}$$

Need to define $\underline{\underline{\sigma}}$'s.

1) Stresses in the pore fluid

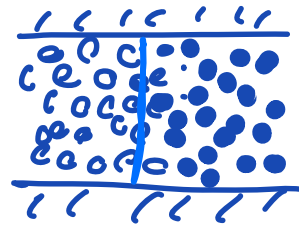
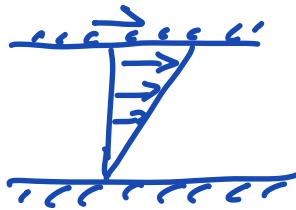
General stress tensor

\sim

$$\underline{\underline{\sigma}}_f = p_f \underline{\underline{I}} + \underline{\underline{\tau}}_f$$

Pore fluid does not accommodate deviatoric stress

$$\underline{\underline{\tau}}_f = \underline{\underline{0}}$$



$$\underline{\underline{\sigma}}_f = -p_f \underline{\underline{I}}$$

p_f = fluid pressure

Need to show that this reduces the lin. mom. balance in the fluid down to Darcy's law.

$$\mathbf{q}_r = \phi (\mathbf{v}_f - \mathbf{v}_s) = -\frac{k}{\mu_f} (\nabla p_f + \rho_f g \hat{z})$$

Start with lin. mom. balance in fluid:

$$\nabla \cdot [\phi \underline{\underline{\sigma}}_f] - \phi \rho_f g \hat{z} - \underline{\underline{f}}_f = 0$$

Need an expression for interaction force

$$\underline{f}_I = c(\underline{v}_f - \underline{v}_s) - p_I \nabla \phi \quad p_I = \text{interface pressure}$$

Simplest expression that is Galilean invariant.

First term is its viscous interaction, \rightarrow drag
Second term is due to pressure acting ~~to~~ on the interface. Necessary to allow for no motion in the case of hydrostatic equilibrium.

Note: Authors differ on choice of p_I :

$$\text{McKenzie (1984): } p_I = p_f$$

$$\text{Bercovici et al (2001): } p_I = (1-\phi)p_f + \phi p_s$$

Here we choose $p_I = p_f$.

3 eqns:

$$\text{lin mom. bal.: } \nabla \cdot [\phi \underline{\underline{s}}_f] - \phi p_f g \hat{z} - \underline{f}_I = 0$$

$$\text{Cauchy stress: } \underline{\underline{s}}_f = -p_f \underline{I}$$

$$\text{interaction force: } \underline{f}_I = c(\underline{v}_f - \underline{v}_s) - p_f \nabla \phi$$

$$-\nabla \cdot (\phi p_f \underline{\underline{I}}) - \phi p_f g \hat{z} - c (\underline{v}_f - \underline{v}_s) + p_f \nabla \phi = 0$$

$$\nabla(\phi p_f) = \phi \nabla p_f + p_f \nabla \phi$$

$$-\phi \nabla p_f - \cancel{p_f \nabla \phi} - \phi p_f g \hat{z} - c (\underline{v}_f - \underline{v}_s) + \cancel{p_f \nabla \phi} = 0$$

$$c (\underline{v}_f - \underline{v}_s) = -\phi (\nabla p_f + p_f g \hat{z})$$

$$\phi (\underline{v}_f - \underline{v}_s) = -\left(\frac{\phi^2}{c}\right) (\nabla p_f + p_f g \hat{z})$$

compare to Darcy's law:

$$\phi (\underline{v}_f - \underline{v}_s) = -\left(\frac{k}{\mu_f}\right) (\nabla p_f + p_f g \hat{z})$$

$$\Rightarrow \underline{\underline{c}} = \frac{k}{\mu_f} \quad \boxed{c = \frac{\phi^2 \mu_f}{k}}$$

$$\Rightarrow \text{interaction force: } \boxed{f_I = \frac{\phi^2 \mu_f}{k} (\underline{v}_f - \underline{v}_s) - p_f \nabla \phi}$$

Our formulation is consistent with Darcy's law.

2) Stress in viscous fluid

General Newtonian ^{stress} tensor is

$$\underline{\underline{\sigma}}_s = -p_s \underline{\underline{I}} + \cancel{\lambda_s \nabla \cdot \underline{v}} \underline{\underline{I}} + 2\mu \underline{\underline{\dot{\epsilon}}}_s$$

but because solid is not compressible itself

$$\lambda_s = 0 \quad \text{but} \quad \nabla \cdot \underline{v}_s \neq 0$$

$$\underline{\underline{\sigma}}_s = - p_s \underline{\underline{I}} + \underline{\underline{T}}_s$$

$$= - p_s \underline{\underline{I}} + \mu_s (\nabla \underline{v} + \nabla^T \underline{v} - \frac{2}{3} \nabla \cdot \underline{v} \underline{\underline{I}})$$

substitute

$$\nabla \cdot [\phi \underline{\underline{\sigma}}_f + (1-\phi) \underline{\underline{\sigma}}_s] = \bar{\rho} g \hat{z}$$

$$\nabla \cdot [-\phi p_f \underline{\underline{I}} - (1-\phi) p_s \underline{\underline{I}} + (1-\phi) \mu_s (\nabla \underline{v} + \nabla^T \underline{v}) - (1-\phi) \mu_s \frac{2}{3} \nabla \cdot \underline{v} \underline{\underline{I}}] = \bar{\rho} g \hat{z}$$

$$\mu_s^* = (1-\phi) \mu_s$$

$$\nabla \cdot [-(\phi p_f + (1-\phi) p_s) \underline{\underline{I}} - \mu_s^* \frac{2}{3} \nabla \cdot \underline{v} \underline{\underline{I}} + \mu_s^* (\nabla \underline{v} + \nabla^T \underline{v})] = \bar{\rho} g \hat{z}$$

introduce compaction relation

$$p_f - p_s = \frac{G \mu_s}{\phi^m} \nabla \cdot \underline{v}_s \quad p_s = p_f - \frac{G \mu_s}{\phi^m} \nabla \cdot \underline{v}_s$$

$$\phi p_f + (1-\phi) p_s = \phi p_f + (1-\phi) (p_f - \frac{G \mu_s}{\phi^m} \nabla \cdot \underline{v}_s)$$

$$= \cancel{\phi p_f} + p_f - \cancel{\phi p_f} + \frac{(1-\phi)}{\phi^m} G \mu_s \nabla \cdot \underline{v}_s$$

$$= p_f - \underbrace{\frac{1-\phi}{\phi^m} G \mu_s}_{S_\phi} \nabla \cdot \underline{v}_s$$

$$= p_f - S_\phi \nabla \cdot \underline{v}_s$$

$$\nabla \cdot \left[\underbrace{-(p_f - S_\phi \nabla \cdot \underline{v}_s)}_{\text{scalar}} \underline{\underline{I}} + \mu_s^* (\nabla \underline{v} + \nabla \underline{v}^T) \right] = \bar{p} g \hat{z}$$

$$\nabla \cdot [\mu_s^* (\nabla \underline{v} + \nabla \underline{v}^T)] - \nabla (p_f - S_\phi \nabla \cdot \underline{v}_s) = \bar{p} g \hat{z}$$

$$S_\phi = \frac{1-\phi}{\phi^n} G \mu_s$$

⇒ Total momentum balance for 2 phase system has same form as for single phase compressible fluid mom. balance.