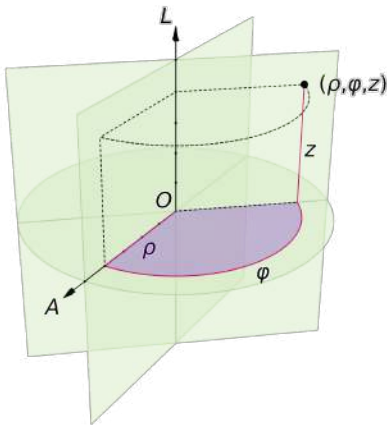


# Non Cartesian Coordinates (1D)

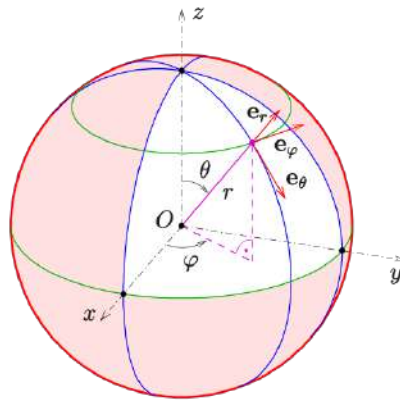
```
clear, close all, clc
set_defaults()
```

The advantage of the dyadic notation ( $\nabla$ ,  $\nabla \cdot$ ,  $\nabla \times$ ) is that it hides the coordinate system. Here we show that the same can be achieved by the discrete operators. Currently we have only discretized one coordinate direction, but this already allows three different coordinate systems

- linear (1D)
- cylindrical radial (2D)
- spherical radial (3D)



Cylindrical Coordinates



Spherical Coordinates

The *gradient* is identical in all three coordinate systems:  $\nabla = \frac{d}{dx}$

Here we also use the independent variable  $x$  to denote the **radial direction** in 2D and 3D.

In contrast to the gradient the *divergence* changes with the coordinate system

- linear (1D):  $\nabla \cdot = \frac{d}{dx}$
- cylindrical radial (2D):  $\nabla \cdot = \frac{1}{x} \frac{d}{dx} x$
- spherical radial (3D):  $\nabla \cdot = \frac{1}{x^2} \frac{d}{dx} x^2$

Therefore we can write the general radial divergence in  $d$  dimensions as:  $\nabla \cdot = \frac{1}{x^{(d-1)}} \frac{d}{dx} x^{(d-1)}$

## Geometric interpretation of the radius terms

The key to the correct discretization is the geometric understanding of the two radius terms in the divergence. To facilitate this consider the equation for one-dimensional incompressible groundwater flow

in compact dyadic notation  $-\nabla \cdot [K\nabla h] = f_s$

or written explicitly in terms of the radial coordinate  $-\frac{d}{dx} \left[ x^{(d-1)} K \frac{dh}{dx} \right] = x^{(d-1)} f_s$ .

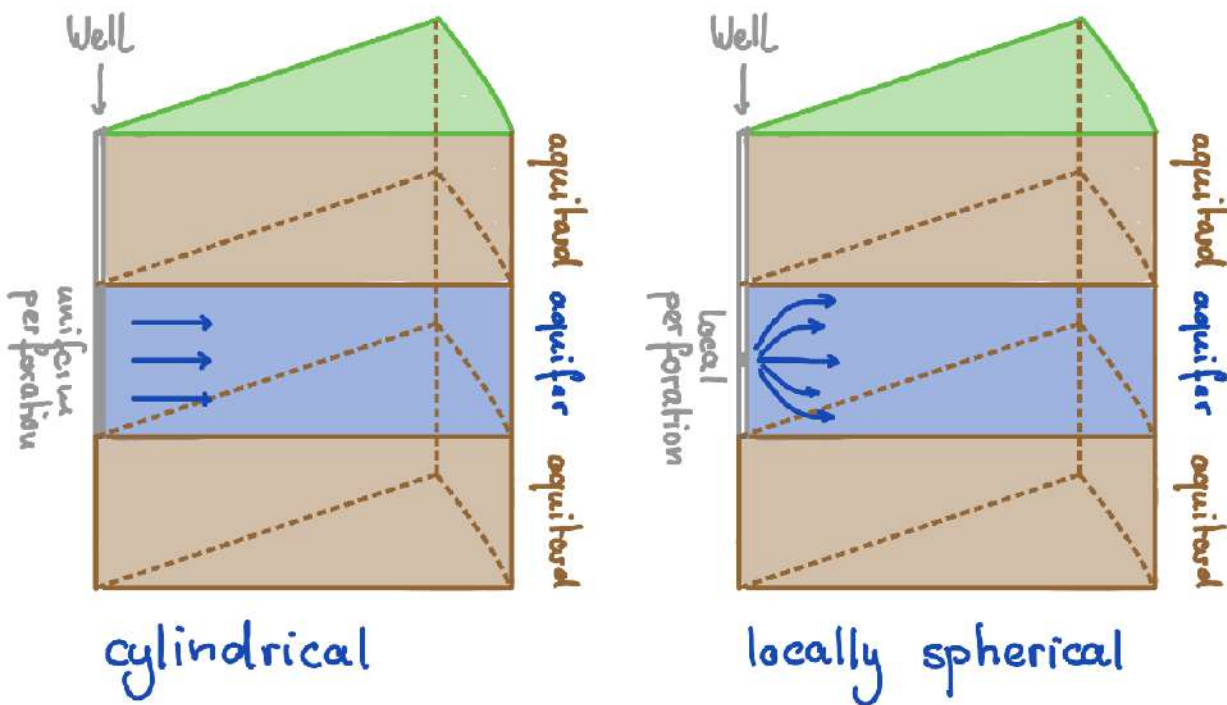
Note, here we have multiplied through by  $x^{(d-1)}$ , so that it is on the right hand side. In this form, the geometric origin of the two radius terms becomes clearer.

- The term  $x^{(d-1)} K$  suggests that this  $x^{(d-1)}$  represents that growth of the interfacial area with increasing radius, because  $K$  is associated with the flux. This radius term should therefore be evaluated at the cell faces  $\text{Grid} \cdot x_f$ .
- The term  $x^{(d-1)} f_s$  suggests that this  $x^{(d-1)}$  represents the growth of the volume with increasing radius, because  $f_s$  is the volumetric source term. This radius term should therefore be evaluated at the cell centers  $\text{Grid} \cdot x_c$ .

## Test problem 1: Steady state flow near a well

Flow near a groundwater well is a common problem in hydrogeology. The well typically has a casing, i.e., a steel tube, that prevents water leakage from formations above the aquifer. In the aquifer the casing is perforated, i.e., has holes, to allow groundwater to enter or exit the well. The near well flow depends on the distribution of perforations in the aquifer interval of the well:

1. Well is **uniformly** perforated over the entire aquifer interval (left) for that water can flow across the entire height so that the flow has **cylindrical** geometry.
2. Well is only **locally** perforated (right). If this local perforation is in the center of the aquifer interval the near well flow has **spherical** geometry.



The cylindrical case is similar to the injection well problem we considered in Lecture 3. Except here we prescribe the head at the well instead of the flow rate.

The problem statement for the near well flow is given by

$$\text{PDE: } -\frac{1}{x^{(d-1)}} \frac{d}{dx} \left[ x^{(d-1)} K \frac{dh}{dx} \right] = 0 \text{ for } x \in [x_{min}, x_{max}]$$

with the Dirichlet BC's  $h(x_{min}) = h_1$  and  $h(x_{max}) = h_2$ , where  $x_{min} > 0$ .

The analytic solutions for the head are given by

- linear (1D):  $h(x) = h_1 + \frac{h_2 - h_1}{x_{max} - x_{min}} (x - x_{min})$
- cylindrical (2D):  $h(x) = h_1 + (h_2 - h_1) \frac{\ln(x/x_{min})}{\ln(x_{max}/x_{min})}$
- spherical (3D):  $h(x) = h_1 + \frac{h_2 - h_1}{\frac{1}{x_{max}} - \frac{1}{x_{min}}} \left( \frac{1}{x} - \frac{1}{x_{min}} \right)$

The corresponding fluxes are given by

- linear (1D):  $q(x) = -K \frac{h_2 - h_1}{x_{max} - x_{min}}$

- cylindrical (2D):  $q(x) = -K \frac{h_2 - h_1}{\ln\left(\frac{x_{max}}{x_{min}}\right)} \frac{1}{x}$
- spherical (3D):  $q(x) = K \frac{h_2 - h_1}{\frac{1}{x_{max}} - \frac{1}{x_{min}}} \frac{1}{x^2}$

We assume the following values, we use the ana

```
cm2m = 1/100;          % cm to m conversion
yr2s = 365*24*60^2;   % yr to s conversion

xmin = .5;            % well radius
xmax = 100;          % domain radius
h2 = 1;              % far-field head
Qw = 1;              % well flow rate
H = 1;              % aquifer thickness
K = 1;              % hydraulic conductivity
Aw = 2*pi*xmin*H;    % wellbore area
% rlim = [param.rw,param.r0];

ha = @(x) h2 - Qw/2/pi/H/K * log(x/xmin);
```

Here we use the analytic solution from class to compute the head at the well from the flow rate

```
h1 = ha(xmin);
h2 = 0;
xana = linspace(xmin-1e-2,xmax,1e3);
h1d_ana = @(x) h1 + (h2-h1)/(xmax-xmin)*(x-xmin);
h2d_ana = @(x) h1 + (h2-h1)*log(x/xmin)/log(xmax/xmin);
h3d_ana = @(x) h1 + (h2-h1)/(1/xmax-1/xmin)*(1./x-1/xmin);

q1d_ana = @(x) -K*(h2-h1)/(xmax-xmin)+x*0;
q2d_ana = @(x) -K*(h2-h1)/log(xmax/xmin)*1./x;
q3d_ana = @(x) K*(h2-h1)/(1/xmax-1/xmin)*1./(x.^2);
```

## Discretization of the divergence

The radial component of the discrete divergence matrix in cylindrical and spherical geometry can therefore be obtained as follows

```
Grid.xmin = xmin; Grid.xmax = xmax; Grid.Nx = 35;
Grid = build_grid(Grid);
[D,G,C,I,M] = build_ops(Grid);
fs = spalloc(Grid.Nx,1,0);

% General radial coordinate system
Rinv = @(d) spdiags(1./Grid.xc.^(d-1),0,Grid.Nx,Grid.Nx);
R = @(d) spdiags(Grid.xf.^(d-1),0,Grid.Nfx,Grid.Nfx);
```

```

D = @(d) Rinv(d)*D*R(d);
L = @(d) -D(d)*K*G;
flux = @(h) -K*G*h;
L1 = L(1); res1d = @(h,cell) L1(cell,:)*h - fs(cell);
L2 = L(2); res2d = @(h,cell) L2(cell,:)*h - fs(cell);
L3 = L(3); res3d = @(h,cell) L3(cell,:)*h - fs(cell);

```

Set Dirichlet boundary conditions

```

BC.dof_dir = [Grid.dof_xmin;Grid.dof_xmax];
BC.dof_f_dir = [Grid.dof_f_xmin;Grid.dof_f_xmax];
BC.dof_neu = [];
BC.dof_f_neu = [];

% 1D - linear
BC.g = h1d_ana(Grid.xc(BC.dof_dir));
[B,N,fn] = build_bnd(BC,Grid,I);
h1d = solve_lbvp(L(1),fs+fn,B,BC.g,N);
q1d = comp_flux_gen(flux,res1d,h1d,Grid,BC);

% 2D - cylindrical
Grid.geom = 'cylindrical_r'; Grid = build_grid(Grid); % update Grid.A and Grid.V
BC.g = h2d_ana(Grid.xc(BC.dof_dir));
h2d = solve_lbvp(L(2),fs+fn,B,BC.g,N);
q2d = comp_flux_gen(flux,res2d,h2d,Grid,BC);

% 3D - spherical
Grid.geom = 'spherical_r'; Grid = build_grid(Grid); % update Grid.A and Grid.V
BC.g = h3d_ana(Grid.xc(BC.dof_dir));
h3d = solve_lbvp(L(3),fs+fn,B,BC.g,N);
q3d = comp_flux_gen(flux,res3d,h3d,Grid,BC);

figure('position',[10 10 1200 600])
subplot 121
plot(xana,h1d_ana(xana),'b-'), hold on
plot(xana,h2d_ana(xana),'r-')
plot(xana,h3d_ana(xana),'k-')
p1 = plot(Grid.xc,h1d,'bo','markerfacecolor','w','markersize',8); hold on
p2 = plot(Grid.xc,h2d,'ro','markerfacecolor','w','markersize',8);
p3 = plot(Grid.xc,h3d,'ko','markerfacecolor','w','markersize',8);
xlabel 'x or r', ylabel 'h'
pbaspect([1 .8 1])
legend([p1 p2 p3],'lin (1D)','cyl (2D)','sph (3D)')

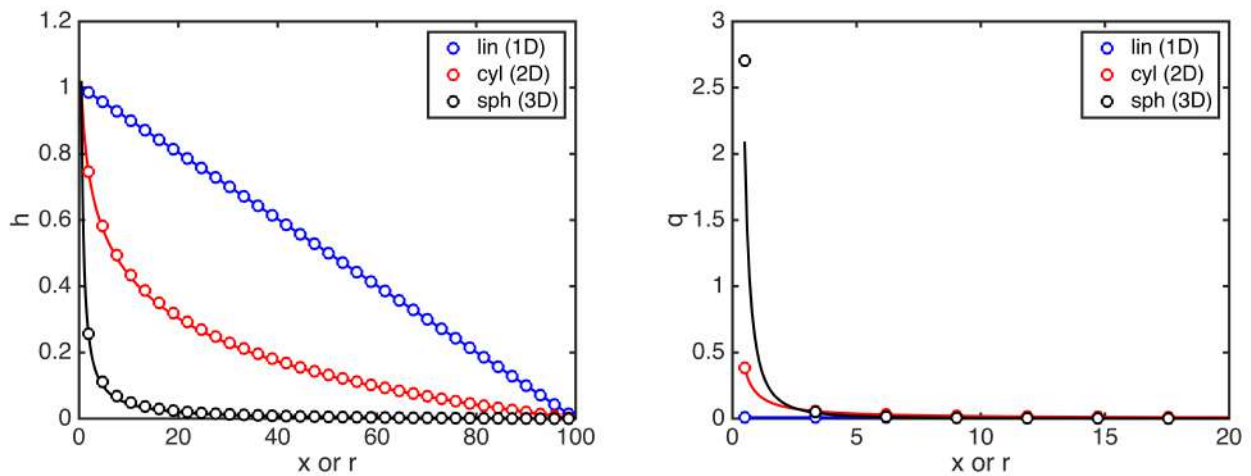
subplot 122
plot(xana,q1d_ana(xana),'b'), hold on
plot(xana,q2d_ana(xana),'r')
plot(xana,q3d_ana(xana),'k')

```

```

l1 = plot(Grid.xf,q1d,'bo','markerfacecolor','w','markersize',8);
l2 = plot(Grid.xf,q2d,'ro','markerfacecolor','w','markersize',8);
l3 = plot(Grid.xf,q3d,'ko','markerfacecolor','w','markersize',8);
xlabel 'x or r', ylabel 'q'
xlim([0 20])
pbaspect([1 .8 1])
legend([l1 l2 l3],'lin (1D)','cyl (2D)','sph (3D)')

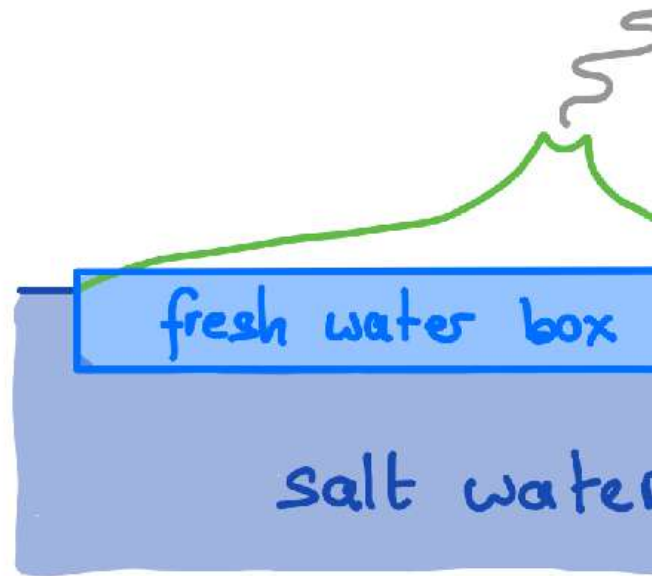
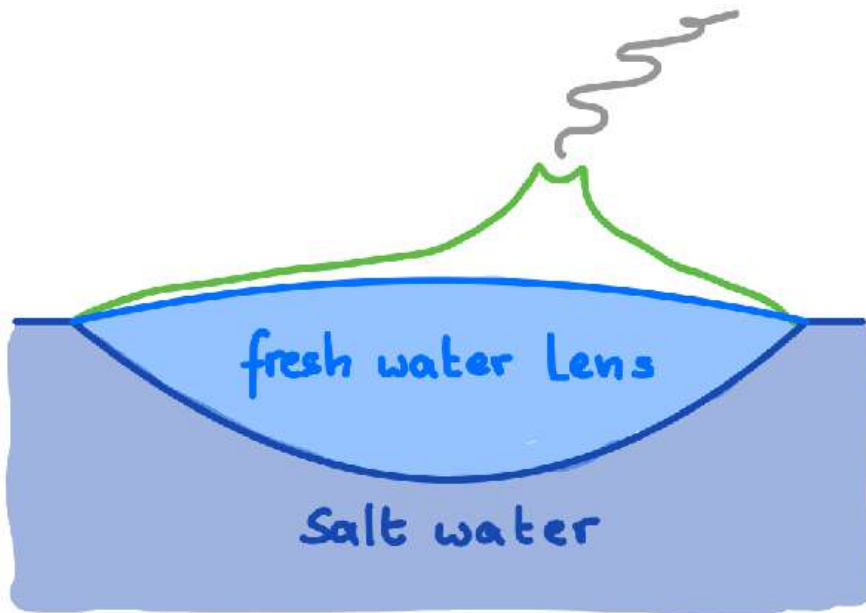
```



If we set the boundary conditions using the analytical solution at the cell centers, the numerical solution matches the analytical solution very well. Our discrete divergence in cylindrical and spherical radial coordinates is therefore correct.

Note how the head decays more rapidly with distance in higher coordinates. This is because the fluid flow is distributed into shells of increasing volume in 2D and 3D.

## Test problem 2: Cylindrical aquifer beneath a (near) circular island



The island of Ihavandhoo (Maledives) has a mean diameter of  $R = 435$  m, an annual rainfall of  $q_p = 1779$  mm and a fresh water lens of approximately  $b = 7$  m thickness. Inhabitants rely on this groundwater and a small desalination plant for all their potable water needs. The real problem of groundwater on islands is complicated because the aquifer is typically unconfined and the fresh water interacts with the denser sea water beneath to form a lens that thins towards the edges of the island. Here we will simply assume that the aquifer is confined and has a rectangular cross-section with average height,  $b$ . The shallow aquifer model is then given by

To compute the steady temperature profile in an asteroid of radius,  $R$ , heated uniformly by radioactive decay we solve

$$-\frac{1}{x} \frac{d}{dx} \left[ x b K \frac{dh}{dx} \right] = q_p \text{ for } x \in [0, R]$$

with the Dirichlet BC  $h(R) = 0$  and the natural (no flow) BC at the center. Note that including the origin,  $r = 0$ , is not a problem because the term  $1/x^{1-d}$  is evaluated at cell centers!

The analytic solution for the head of the island aquifer is given by

$$h(x) = \frac{q_p}{4bK} (R^2 - r^2)$$

The fluid flux in the aquifer is given by

$$q(x) = \frac{q_p}{2b} r.$$

```

R = 435;                % Island radius [m]
K = 2e-2*cm2m;        % Hydraulic conductivity [m/s]
b = 7;                % fresh water lens thickness [m]
qp = 177.9*cm2m/yr2s; % Average annual precipitation [m3/m2/s]

% Analytical solution
xa_island = linspace(0,R,1e3);
ha_island = @(x) qp/(4*b*K)*(R^2-x.^2);
qa_island = @(x) qp/(2*b)*x;

% Numerical solution
Grid.xmin = 0; Grid.xmax = 435; Grid.Nx = 15;
Grid.geom = 'cylindrical_r';
Grid = build_grid(Grid);
[D,G,C,I,M] = build_ops(Grid);
fs = qp/b*ones(Grid.Nx,1);
L = -D*K*G;
flux_island = @(h) -K*G*h;
res_island = @(h,cell) L(cell,:)*h-fs(cell);

% Set boundary conditions
BC.dof_dir = [Grid.dof_xmax];
BC.dof_f_dir = [Grid.dof_f_xmax];
BC.g = ha_island(Grid.xc(BC.dof_dir));
BC.dof_neu = [];
BC.dof_f_neu = [];
BC.qb = [];
[B,N,fn] = build_bnd(BC,Grid,I);

h_island = solve_lbvp(L,fs+fn,B,BC.g,N);
q_island = comp_flux_gen(flux_island,res_island,h_island,Grid,BC);

figure('position',[10 10 1200 600])
subplot 121
plot(xa_island,ha_island(xa_island),'b-'), hold on

```

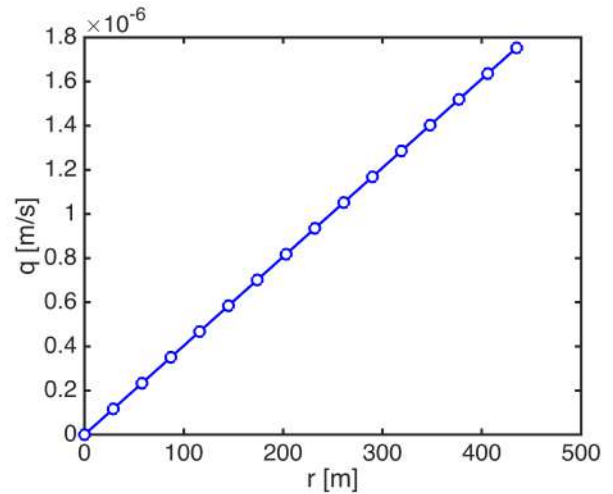
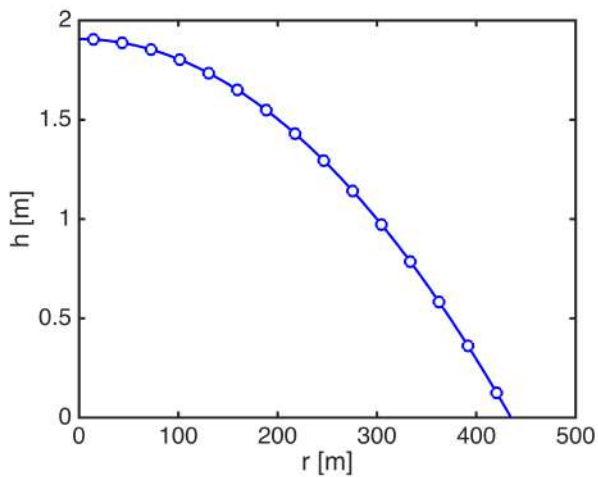


```

plot(Grid.xc,h_island,'bo','markerfacecolor','w','markersize',8)
pbaspect([1 .8 1])
xlabel 'r [m]', ylabel 'h [m]'

subplot 122
plot(xa_island,qa_island(xa_island),'b-'), hold on
plot(Grid.xf,q_island,'bo','markerfacecolor','w','markersize',8), hold on
pbaspect([1 .8 1])
xlabel 'r [m]', ylabel 'q [m/s]'

```



## Auxillary functions

### set\_defaults()

```

function [] = set_defaults()
    set(0, ...
        'defaultaxesfontsize', 18, ...
        'defaultaxeslinewidth', 2.0, ...
        'defaultlinelinewidth', 2.0, ...
        'defaultpatchlinewidth', 2.0, ...
        'DefaultLineMarkerSize', 12.0);
end

```