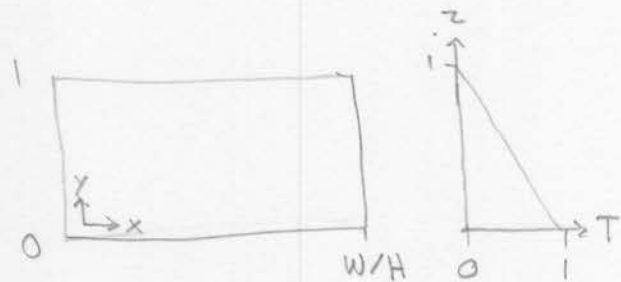


Modeling Stokes Convection

①

Governing Equations

$$\begin{aligned} 1) & \nabla \cdot [\mu (\nabla \underline{v} + \nabla \underline{v}^T)] - \nabla \pi = T \hat{z} \\ 2) & \nabla \cdot \underline{v} = 0 \\ 3) & \frac{\partial T}{\partial t} + \nabla \cdot [\underline{v} T - \frac{1}{Ra} \nabla T] = 0 \end{aligned}$$



Estimates of Rayleigh number in ice: $Ra = \frac{\Delta \rho g H^3}{\mu_c \kappa}$

$$\left. \begin{aligned} \mu_c &= 10^{14} \text{ Pas} \\ g &= 10^0 \text{ m/s}^2 \\ \Delta \rho &= 10^1 \text{ kg/m}^3 \\ \kappa &= 10^{-6} \text{ m}^2/\text{s} \\ H &= 10^4 \text{ m} \end{aligned} \right\} Ra = 10^1 \cdot 10^0 \cdot 10^{(4)^3} \cdot 10^{-14} \cdot 10^6$$
$$= 10^{1+12-14+6} = \underline{\underline{10^5}}$$

$\Rightarrow$ Heat transport is expected to be dominated by advection.

Implementation of the convection code

Need to solve three coupled equations.

1) Flow problem: solve 1 & 2 given T

2) Transport problem: solve 3 given $\underline{v}$

Note, that Transport problem is solved on same grid as pressure $\Rightarrow$ use G_p & D_p for transport.

Note, our problem has only one parameter, Ra .

General code outline

(2)

1) Define physical & numerical parameters

Ra

θ , $t_{\max}$, $dt_{\max}$, cfl , plot/save interval

2) Build grid & ops

- general operators $\rightarrow$ build_stokes_grid/ops

- Stokes operator

- ADE operators

- Boundary conditions.

3) Transient evolution

- define initial condition

T , time, counters (i, k)

- while loop time < $t_{\max}$

• Flow problem: 1) Buoyancy term from T 2) solve stokes

• Transport problem: 1) Determine time step 2) solve transport.

• Plot & save solution:

The following items need discussion:

1) ADE operator

2) Buoyancy term

3) Time step selection

1) Advection-diffusion equation

$$\frac{\partial T}{\partial t} + \nabla \cdot [\underline{v} T - \frac{1}{Ra} \nabla T] = 0$$

since $\underline{u} = [\underline{v} \ p]$ in Stokes problem we'll treat convection and use $\underline{T}$ as solution vector.

We'll use the standard θ -method for time step discretization

$$\underline{T} \frac{T^{n+1} - T^n}{\Delta t} + \underline{Dp} * [\underline{A}(\underline{v}) - \frac{1}{Ra} \underline{Gp}] (\theta T^n + (1-\theta) T^{n+1}) = 0$$

Collect T^{n+1} on lhs and T^n on the rhs.

$$\left(\underline{T} + (1-\theta) \Delta t \underline{Dp} * [\underline{A}(\underline{v}) - \frac{1}{Ra} \underline{Gp}] \right) T^{n+1} = \left(\underline{T} - \theta \Delta t \underline{Dp} * [\underline{A}(\underline{v}) - \frac{1}{Ra} \underline{Gp}] \right) T^n$$

L-trans
L-trans

Hence we have: $\underline{Im_trans} = \underline{T_trans} + (1-\theta) \Delta t * \underline{L_trans}$

$$\underline{Ex_trans} = \underline{T_trans} - \theta \Delta t * \underline{L_trans}$$

↑

just emphasizing this is the identity on p-grid.

Note: These operators change each time step because the flow field changes $\Rightarrow$ anonymous functions

2) Buoyancy term in Stokes Equation

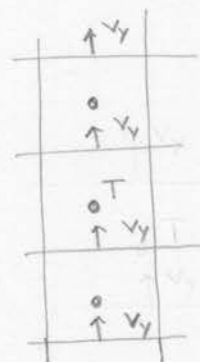
(4)

The new term in Stokes equation

$$\nabla \cdot [\mu(\nabla \underline{v} + \nabla^T \underline{v})] - \nabla \pi = \underline{T} \hat{z}$$

buoyancy term

T is a variable that lives in cell centers but here it is used as body force on the v_z (or v_y) velocity.



Interpolate T to the cell faces

$\Rightarrow$ use comp-mean (with $p=1$ for arithmetic average)

This will give us a diagonal matrix.

Need to extract the diagonal from matrix and then only add the averages on y-faces to rhs.

3) Timestep selection

To minimize numerical diffusion, we are explicitly time stepping the advection-diffusion equation. ($\theta=1$)

Conditional stability requires timestep restriction

1) CFL-condition (advection): $\Delta t < \min(\frac{\Delta x}{v_x}, \frac{\Delta y}{v_y})$

2) Neumann-condition (diffusion): $\Delta t < \min(\frac{Ra \Delta x^2}{2}, \frac{Ra \Delta y^2}{2})$

For high Ra the CFL condition is typically limiting.

Always check both conditions.

Some notes on time step selection:

⑤

- 1) Advancing ADE with known v is a linear problem
 $\Rightarrow$ expect to have a robust max Δt criterion = (cfl-number ~ 0.9)
- 2) CFL & Neumann conditions are applied "direction by direction"
and separately
 $\Rightarrow$ will not give a robust criterion, because different directions and processes can amplify each other.

Right it seems we need a much more restrictive cfl-number
and it seems to change with grid resolution.
= need better criterium.