

## Motivating example: Volcanic heat pipe

```
clc, close all, clear
set_demo_defaults
```

Consider steady heat flow from a volcanic conduit with radius,  $r_c$ , height,  $H_c$ , and a constant rate of heat flow,  $Q_c$ , entering the conduit at the base. Heat leaves the conduit sideways by conduction into the volcanic rock with thermal conductivity  $\kappa$  (assumed to be isotropic and constant). The mean radius of the volcanic construct is  $R$ .

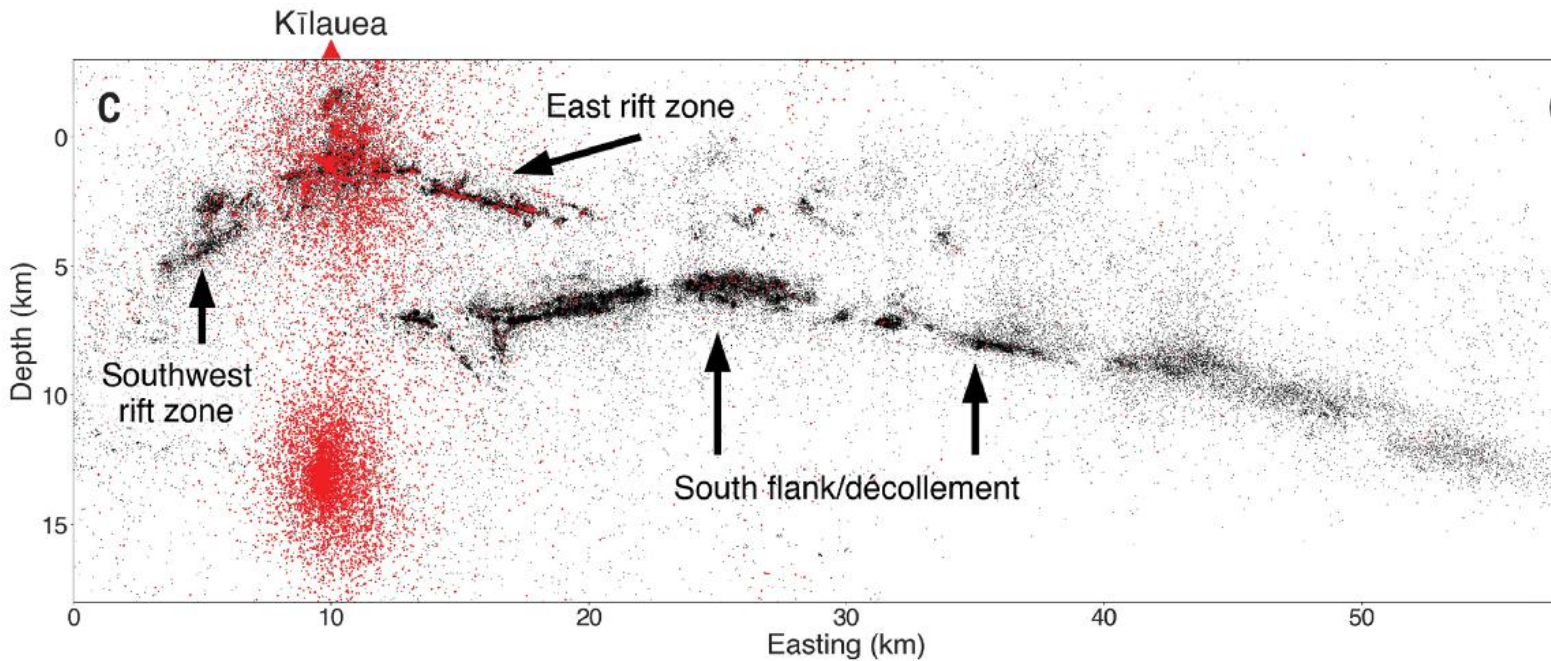


Figure 1: Seismic image of the volcanic conduit beneath Mauna Loa, Hawaii (Wilding et al. 2023)

The steady heat flow equation in coordinate-independent notation is given by

$$-\nabla \cdot [\kappa \nabla T] = f_s$$

where  $f_s$  is a source/sink term assumed to be zero here. Instead we write the PDE in cylindrical coordinates, assuming circumferential

symmetry, and represent the conduit as a boundary condition. The divergence and gradient in radial direction are given by

$$\nabla \cdot = \frac{1}{r} \frac{d}{dr} r(\bullet) \text{ and } \nabla = \frac{d}{dx}$$

so that we have the following problem

$$-\frac{1}{r} \frac{d}{dr} \left[ r \kappa \frac{dT}{dr} \right] = 0 \text{ for } r \in [r_c, R]$$

with the following flux boundary condition at the conduit

$$Q_c = A_c q_r(r = r_c) = -A_c \kappa \left. \frac{dT}{dr} \right|_{r=r_c}$$

where  $A_c = 2\pi r_c H_c$  is the area of the surface area of the conduit. This gives a condition on the derivative of  $T$  at the well

$$\left. \frac{dh}{dr} \right|_{r=r_w} = -\frac{Q_w}{A_w K}$$

At the surface of the volcanic construct we assume a constant surface temperature  $T(r = R) = T_s$ . The parameter values below are only for illustrative purposes.

```
% Physical Properties (gleaned from Figure)
param.rc = 1e3;      % [m] conduit radius
param.R = 6e4;      % [m] volcano radius
param.Ts = 25;     % [C] Surface temperature
param.Qc = 5e7;    % [J/s] Rate of heat flow (I have simply chosen this to
give a 'magmatic' T at the conduit)
param.Hc = 1.5e4;  % [m] Conduit height
param.kappa = 2.7; % [W/m/K] thermal conductivity of basalt (Halbert and
Parnell 2022)

% Derived quantities
param.Aw = 2*pi*param.rc*param.Hc; % wellbore area
rlim = [param.rc,param.R];
```

## Analytic solution

The analytic solution for this problem is obtained by integrating twice and is given by

$$T(r) = T_s - \frac{Q_c}{2\pi H_c \kappa} \ln\left(\frac{r}{R}\right),$$

$$q_r(r) = \frac{Q_c}{2\pi H_c} \frac{1}{r},$$

$$Q(r) = Q_c,$$

The particular solution for the parameter values given above is shown in the first figure.

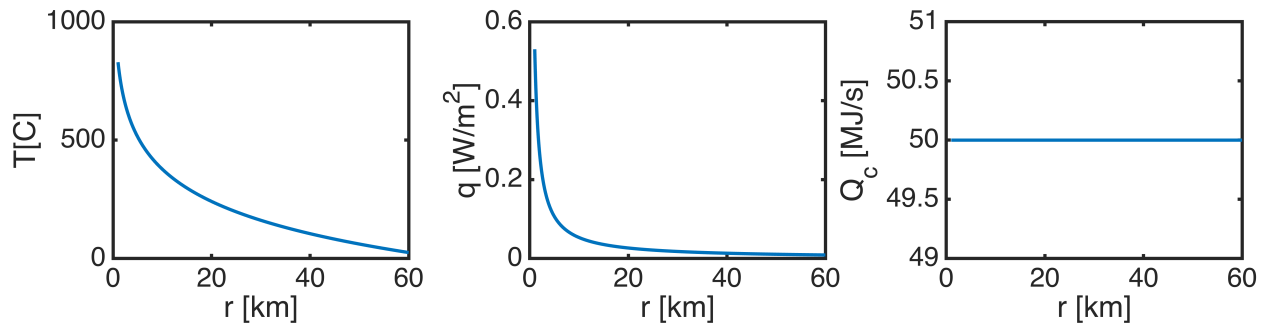
```
[xa,ua,qa,Qa] = AnalyticSolution(param);

figure('position',[10 10 900 500])
subplot 131
plot(xa/1e3,ua(xa),'-');
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'T[C]'
subplot 132
plot(xa/1e3,qa(xa),'-')
pbaspect([1 .8 1])
```

```

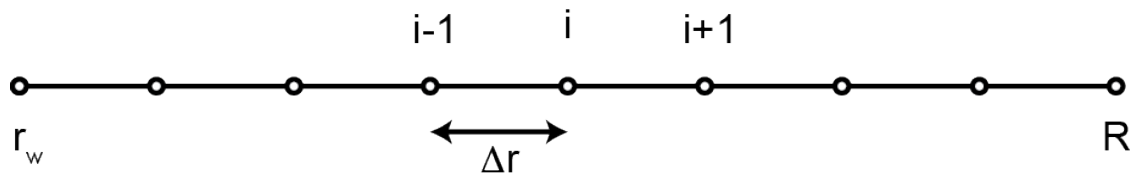
xlabel 'r [km]', ylabel 'q [W/m^2]'
subplot 133
plot(xa/1e3,Qa(xa)/1e6,'-')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'Q_c [MJ/s]'

```



This is a challenging solution due to the strong boundary layer at the well where the gradient of  $T$  becomes very steep.

## 1) Standard finite difference approximation



Above is a standard finite difference grid with node spacing  $\Delta r$  and node index  $i$ . To use standard finite difference approximations for the first and second derivative we first need to expand the divergence

$$\frac{d}{dr} \left[ r \frac{dT}{dr} \right] = r \frac{d^2 T}{dr^2} + \frac{dT}{dr}$$

Then we can use the differentiation matrix,  $\mathbf{D}$ , to approximate the PDE as follows

$$r \frac{d^2 T}{dr^2} + \frac{dT}{dr} \approx [\mathbf{R} * \mathbf{D}^2 + \mathbf{D}] * \mathbf{u}$$

where  $\mathbf{R}$  is a diagonal matrix containing the position of the nodes and  $\mathbf{u}$  is the discrete solution vector. This numerical solution is shown below.

```

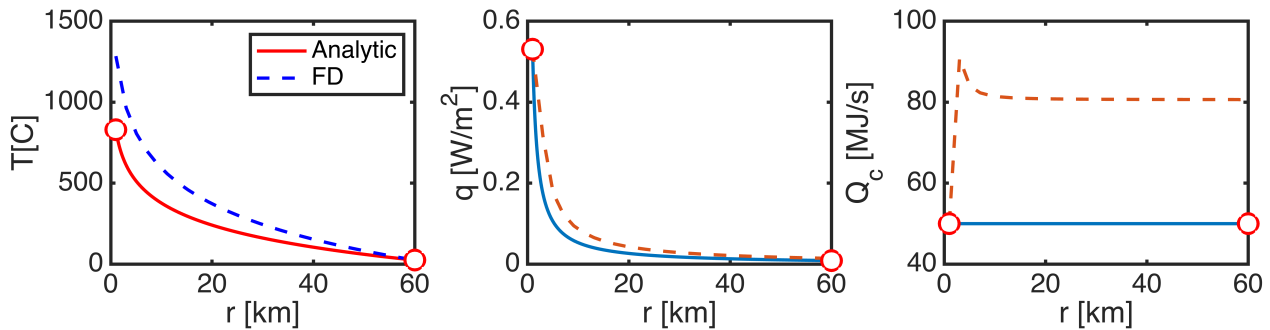
param.Nx = 30; param.BC = 'ND';
[xFD,uFD,qFD,QFD] = FiniteDifferenceSolution(param,ua);

figure('position',[10 10 900 500])
subplot 131
plot(xa/1e3,ua(xa),'r-',xFD/1e3,uFD,'b--'); hold on
plot(rlim/1e3,ua(rlim),'o','markerfacecolor','w','markeredgecolor','r')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'T[C]'
legend('Analytic','FD')

subplot 132
title 'Standard finite differences'
plot(xa/1e3,qa(xa),'-',xFD/1e3,qFD,'--'), hold on
plot(rlim/1e3,qa(rlim),'o','markerfacecolor','w','markeredgecolor','r')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'q [W/m^2]'

subplot 133
plot(xa/1e3,Qa(xa)/1e6,'-',xFD/1e3,QFD/1e6,'--'), hold on
plot(rlim/1e3,Qa(rlim)/1e6,'o','markerfacecolor','w','markeredgecolor','r')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'Q_c [MJ/s]'

```



drawnow

Observations:

1. Standard finite differences lead to surprisingly large errors on the head, because we need to resolve the thin boundary layer near the well.
2. The flow rate,  $Q$ , is not constant! **The mass of pore fluid is not conserved.** This will lead to wrong transport speeds for any solutes carried by fluid.

Of course the solution will converge if the grid is refined sufficiently and mass balance errors will asymptote to zero. However, in practical simulations (2D or 3D) it is typically not possible to refine the grid sufficiently to obtain acceptable errors.

## 2) Finite differencing in conservation form

In particular the coupling between transport of solutes or energy and fluid flow requires that the numerical solution maintains discrete conservation. We lose the mass conservation in the standard finite difference discretization because we expand the divergence using the product rule. **We need to discretize the equation with the divergence intact.**

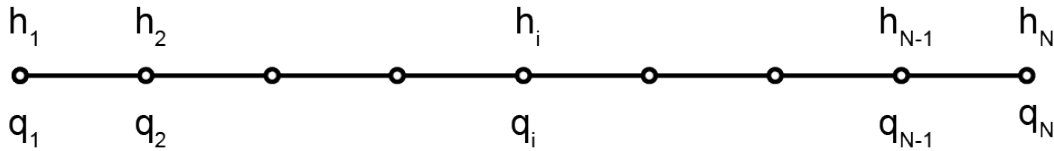
$$-\nabla \cdot [K \nabla h] = -\frac{1}{r} \frac{d}{dr} \left[ r K \frac{dh}{dr} \right] = 0$$

It helps to rewrite the *second-order* equation as a 'div-grad system' of two *first-order* equations for the head,  $h$ , and the radial component of the flux,  $q_r$ , as

$$1. \nabla \cdot \mathbf{q} = \frac{1}{r} \frac{d}{dr} [r q_r] = 0$$

$$2. q_r = -K \nabla h = -K \frac{dh}{dr}$$

We discretize these equations on a co-located grid, where both  $\mathbf{h} = h(\mathbf{x})$  and  $\mathbf{q} = q_r(\mathbf{x})$  are approximated at the same nodes.



So we approximate the two first-order equations as

$$1. \frac{d}{dr} [r q_r] \approx \frac{r_{i+1} q_{i+1} - r_{i-1} q_{i-1}}{2\Delta r}, D^* R^* q$$

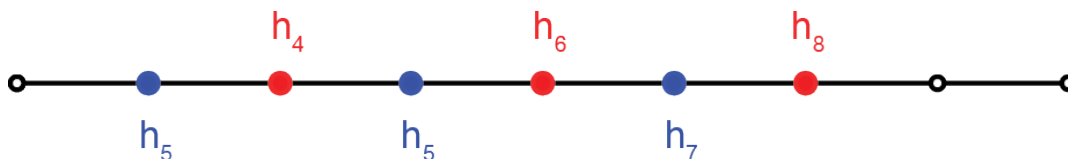
$$2. -K \frac{dh}{dr} \approx K_i \frac{h_{i+1} - h_{i-1}}{2\Delta r} = q_i. q = -K^* D^* h$$

$D^*[R^*D^*h]$

We can eliminate  $q_i$  by substituting 2 into 1 to obtain

$$-\frac{1}{4\Delta r^2} [r_{i+1} K_{i+1} h_{i+2} - (r_{i+1} K_{i+1} + r_{i-1} K_{i-1}) h_i + r_{i-1} K_{i-1} h_{i-2}]$$

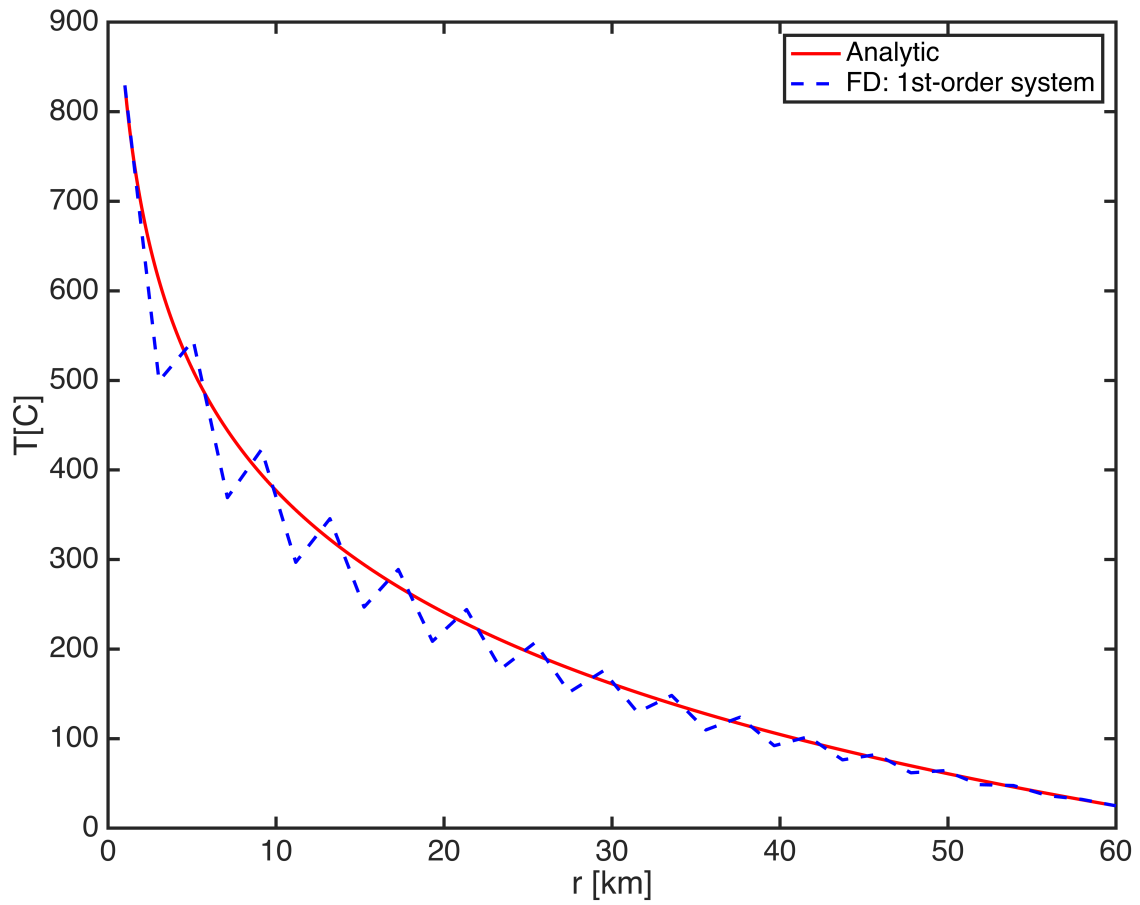
this *stencil* involves  $h_{i-2}$ ,  $h_i$  and  $h_{i+2}$  and leads to a decoupling of the even and odd nodes



```
param.Nx = 30;
[x,u,q,Q,L,L_e_o] = FD_collocated(param,ua);

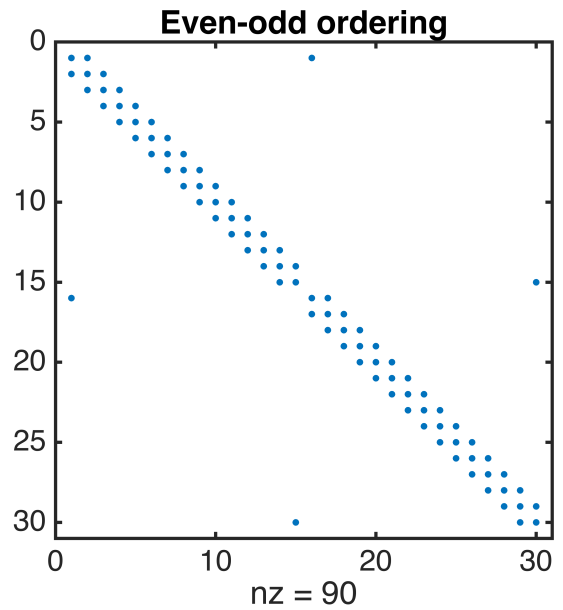
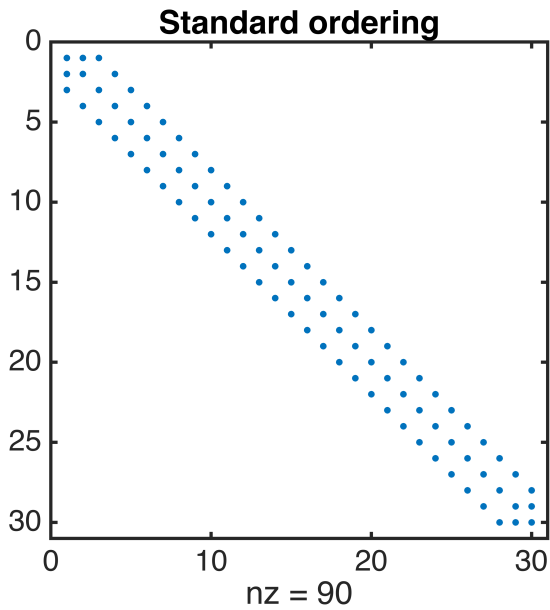
figure('position',[10 10 900 600])
plot(xa/1e3,ua(xa),'r-'); hold on
plot(x/1e3,u,'b--')
xlabel 'r [km]', ylabel 'T[C]'

pbaspect([1 .8 1])
legend('Analytic','FD: 1st-order system')
```



This decoupling leads to oscillations between even and odd nodes.

```
figure('position',[10 10 900 600])
subplot 121
spy(L)
title 'Standard ordering'
subplot 122
spy(L_e_o)
title 'Even-odd ordering'
```



### 3) Conservative Finite Differences (CFD)

Third time is the charm (hopefully). We stay with the equations in the 'div-grad form':

$$1. \quad \nabla \cdot \mathbf{q} = \frac{1}{r} \frac{d}{dr} [r q_r] = 0$$

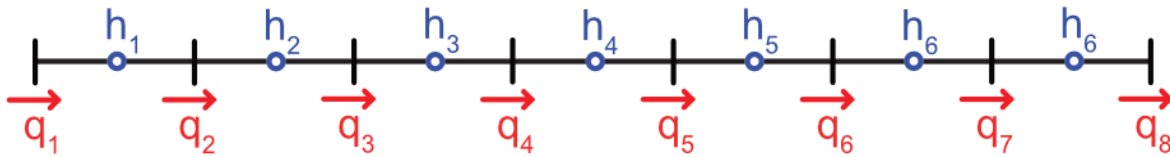
$$2. \quad q_r = -\kappa \nabla T = -\kappa \frac{dT}{dr}$$

However, we change from the **collocated** grid to a **staggered** grid to avoid the decoupling of the even and odd degrees of freedom.

On a staggered grid, where  $\mathbf{u} = T(\mathbf{x}_c)$  and  $\mathbf{q} = q_r(\mathbf{x}_f)$  are approximated at the different locations. We divide the domain into equal cells

and approximate the heads,  $\mathbf{u}$ , at the cell centers,  $\mathbf{x}_c$ , but approximate the fluxes,  $\mathbf{q}$ , at cell faces,  $\mathbf{x}_f$ .





```

param.Nx = 100;
% param.BC = 'DD';
% param.BC = 'DD2';
param.BC = 'ND';

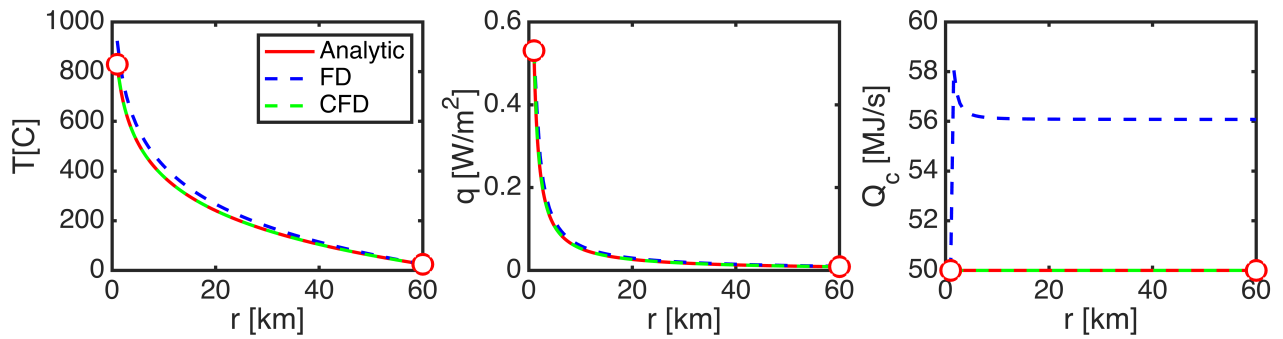
[xa,ua,qa,Qa] = AnalyticSolution(param);
[xFD,uFD,qFD,QFD] = FiniteDifferenceSolution(param,ua);
[xc,xf,uFV,qFV,QFV] = FiniteVolumeSolution(param,ua);

figure('position',[10 10 900 600])
subplot 131
plot(xa/1e3,ua(xa),'r-',xFD/1e3,uFD,'b--',xc/1e3,uFV,'g--'); hold on
plot(rlim/1e3,ua(rlim),'o','markerfacecolor','w','markeredgecolor','r')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'T[C]'
legend('Analytic','FD','CFD')

subplot 132
plot(xa/1e3,qa(xa),'r-',xFD/1e3,qFD,'b--',xf/1e3,qFV,'g--'), hold on
plot(rlim/1e3,qa(rlim),'o','markerfacecolor','w','markeredgecolor','r')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'q [W/m^2]'

subplot 133
plot(xa/1e3,Qa(xa)/1e6,'r-',xFD/1e3,QFD/1e6,'b--',xf/1e3,QFV/1e6,'g--'),
hold on
plot(rlim/1e3,Qa(rlim)/1e6,'o','markerfacecolor','w','markeredgecolor','r')
pbaspect([1 .8 1])
xlabel 'r [km]', ylabel 'Q_c [MJ/s]'

```



### Auxillary functions

```
function [xa,ha,qa,Qa] = AnalyticSolution(param)
rw = param.rc;
r0 = param.R;
h0 = param.Ts;
Qw = param.Qc;
H = param.Hc;
K = param.kappa;

% Analytic solution
xa = linspace(rw,r0,1e3);
ha = @(r) h0 - Qw/2/pi/H/K * log(r/r0);
qa = @(r) Qw/2/pi/H./r;
Qa = @(r) Qw+0*r;
end
```

```
%% Finite difference solution
function [xFD,hFD,qFD,QFD] = FiniteDifferenceSolution(param,ha)
```

```

rw = param.rc;
r0 = param.R;
h0 = param.Ts;
Qw = param.Qc;
H = param.Hc;
K = param.kappa;
Nx = param.Nx;
BC = param.BC;
Aw = param.Aw;

x = linspace(rw,r0,Nx)'; dx = x(2)-x(1);
e = ones(Nx,1);
D = spdiags([-e e]/2/dx,[-1 1],Nx,Nx);
D(1,1) = -3/2/dx; D(1,2) = 4/2/dx; D(1,3) = -1/2/dx;
D(Nx,Nx) = 3/2/dx; D(Nx,Nx-1) = -4/2/dx; D(Nx,Nx-2) = 1/2/dx;

D2 = spdiags([e -2*e e]/dx^2,[-1 0 1],Nx,Nx);
R = spdiags(x,0,Nx,Nx); I = speye(Nx,Nx);
L = -K*(R*D2+D); fs = zeros(Nx,1);

if strcmp(BC,'ND')
    L(1,:) = D(1,:); fs(1) = -Qw/Aw/K;
    B = I(Nx,:); N = I; N(:,Nx) = [];
    g = ha(r0);
elseif strcmp(BC,'DD') || strcmp(BC,'DD2')
    B = I([1;Nx],:); N = I; N(:,[1;Nx]) = [];
    g = [ha(rw);ha(r0)];
end

hFD = solve_lbvvp(L,fs,B,g,N);
qFD = -K*D*hFD;
QFD = 2*pi*H*x.*qFD;
xFD = x;
end

```

```

function [x,h,q,Q,L,L_e_o] = FD_collocated(param,ha)
rw = param.rc;
r0 = param.R;
h0 = param.Ts;
Qw = param.Qc;
H = param.Hc;
K = param.kappa;
Nx = param.Nx;
%BC = param.BC;
%Aw = param.Aw;

x = linspace(rw,r0,Nx)'; dx = x(2)-x(1);
e = ones(Nx,1);

```

```

D = full(spdiaigs([-e e]/2/dx,[-1 1],Nx,Nx));
D(1,1) = -1/dx; D(1,2) = 1/dx;
D(Nx,Nx-1) = -1/dx; D(Nx,Nx) = 1/dx;
% D(1,N) = -1/2; D(N,1) = 1/2;
% D = D/dx;

r = spdiags(x,0,Nx,Nx);
L = -D*r*D;

B = zeros(2,Nx); B(1,1) = 1; B(2,Nx) = 1;
I = eye(Nx); N = I(:,2:Nx-1);
g = [ha(rw); ha(r0)];

odd = [1:2:Nx]'; even = [2:2:Nx]';
P = I([odd;even],:);
L_e_o = P*L*P';
% subplot 121
% spy(L)
% title 'Standard ordering'
% subplot 122
% spy(P*L*P')
% title 'Even-odd ordering'

h = solve_lbvvp(L,0,B,g,N);
q = -D*h;
Q = x.*q;

end

```

```

%% Finite volume solution
function [xc,xf,hFV,qFV,QFV] = FiniteVolumeSolution(param,ha)
rw = param.rc;
r0 = param.R;
h0 = param.Ts;
Qw = param.Qc;
H = param.Hc;
K = param.kappa;
Nx = param.Nx;
BC = param.BC;
Aw = param.Aw;

Grid.xmin = rw; Grid.xmax = r0; Grid.Nx = Nx; Grid.geom = 'cylindrical_r';
Grid = build_grid(Grid);

[D,G,C,I,M] = build_ops(Grid);
L = -D*K*G; fs = zeros(Grid.Nx,1); fn = fs;

```

```

if strcmp(BC,'ND')
    %B = I(Grid.Nx,:); N = I; N(:,Nx) = [];
    Param.g = ha(r0-Grid.dx/2);
    %fn(1) = Qw/Grid.V(1);
    Param.dof_dir = [Grid.dof_xmax];
    Param.dof_f_dir = [Grid.dof_f_xmax];
    Param.dof_neu = [Grid.dof_xmin];
    Param.dof_f_neu = [Grid.dof_f_xmin];
    Param.qb = Qw/Aw;
    [B,N,fn] = build_bnd(Param,Grid,I);
    % fn(1) = Qw/Grid.V(1);
elseif strcmp(BC,'DD')
%     B = I([1;Nx],:); N = I; N(:,[1;Nx]) = [];
    Param.g = [ha(rw);ha(r0)];
    Param.dof_dir = [Grid.dof_xmin;Grid.dof_xmax];
    Param.dof_f_dir = [Grid.dof_f_xmin;Grid.dof_f_xmax];
    Param.dof_neu = []; Param.dof_f_neu = [];
    [B,N,fn] = build_bnd_class(Param,Grid);
elseif strcmp(BC,'DD2')
    B = I([1;Nx],:); N = I; N(:,[1;Nx]) = [];
    Param.g = [ha(rw+Grid.dx/2);ha(r0-Grid.dx/2)];
end

hFV = solve_lbvp(L,fs+fn,B,Param.g,N);
%qFV = comp_flux(D,K,G,hFV,fs,Grid);
qFV = comp_flux(D,K,G,hFV,fs,Grid,Param);
QFV = 2*pi*Grid.xf*H.*qFV;
xc = Grid.xc;
xf = Grid.xf;
end

```